

BASS LAKE DITCH

21

FIELD BOOK

1308

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

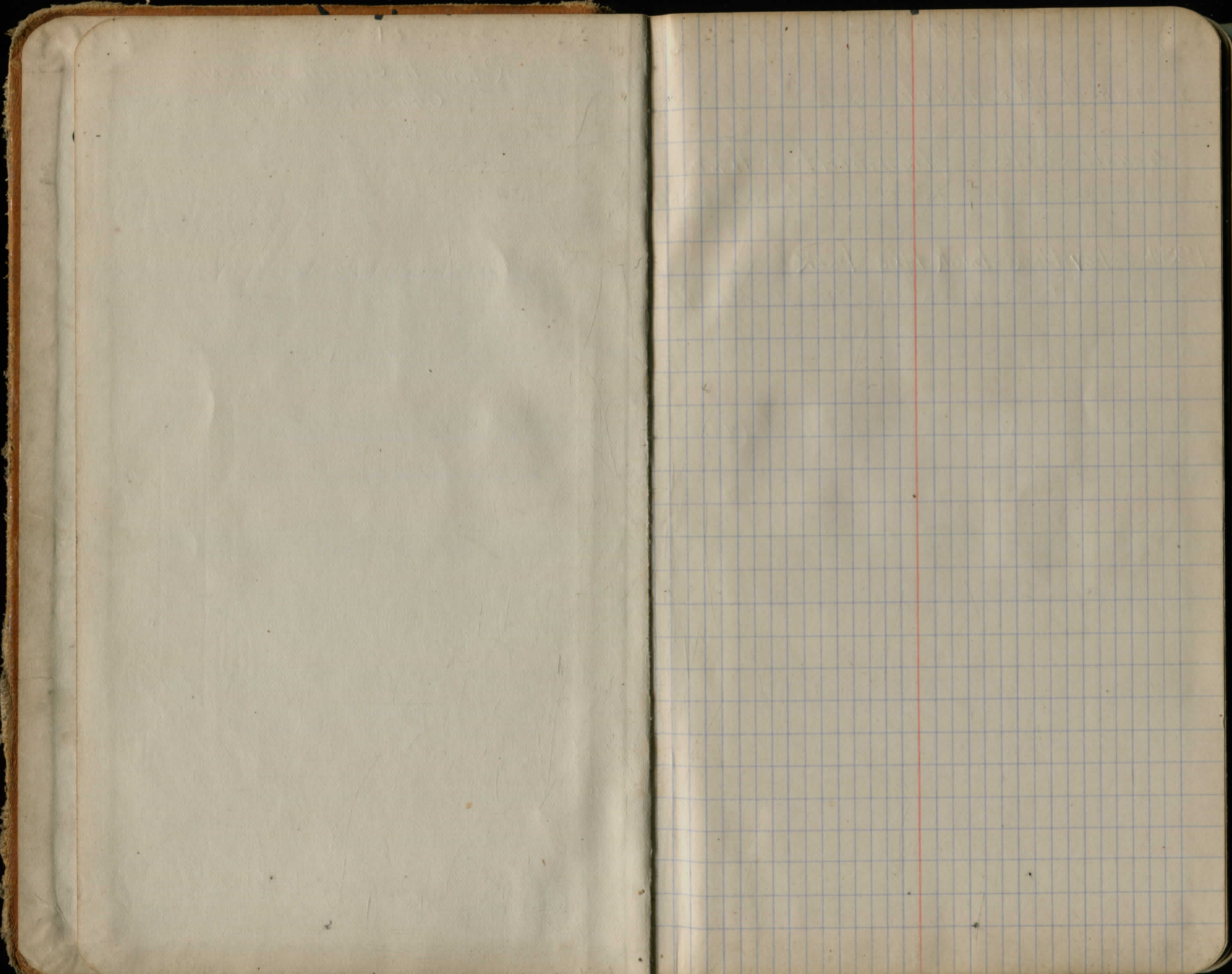
Book 21

Return to County Surveyor
Chardon - Ohio

BASS LAKE DITCH
Entire book

21

note mem. top of page 47 - 96.48 = low
water 8/23/28
"High water" mark = 8/23/28
Loc. 2



INDEX

v

Bass Lake Ditch

Transit Notes - Alignment 4 to 24
Measurements on ice-reference lines 28 & 30

1934 Elevations = back this book

4 December 8th Eff. Fiedler & Ernest Koeney
Bass Lake Ditoh - 1916

STA.

4

approx

3 + 23 Iron pipe on E. & W. prof. Line (4) to L.

3 + 12 2 tacks in 22" Black Ash Tree (19.0)

□ 3 Tangent

2 + 83 2 tacks in 10" Black Ash Tree (18.5)

2 (no stake)

1 (no stake)

0 (no stake) out in lake

Note: Ref. Points are
measured level - & are
usually less than 1 FT.
above ground.

2" Iron pipe

References

"Wood 12"
N. 89°-30' W.

Offset
Line Staked

25'

pitch

Line

□

15'

□

Koeney's

□

Line

6 12/8-1916 - Fiedler & Keeney
Bass Lake Hitch

Sta.

+40

(31.3')

9

+35 old outlet enters from R.

(35')

2 nails in root 16" hard Maple (12.5')

△ 8 24° - 48' Left

+91 2 nails in root 20" hard Maple (12')

+50

+06 2 tacks in 18" Beech Tree (11.0')

△ 7 21° - 10' Left.

+73 2 tacks in 28" Beech Tree (51.0')

6

5



30" Beech spike in root

6+57.5

References to S.E. corner of Osborn Property

Aug. 8, 1934, ...
W.C. Marks
+ F.R. Zethmayer

Pipe set
Pipe Found.
Durell
Pipe Found.
Kinney's Line
Sta. 6
Sta. 5

Σ 12/8-1966 Tindler & Keeney
Bass Lake Ditch

Sta-

13

Kinney's Sta. 13 on R. bank ditch (57.5) (63.3)

12

11

10+62 nail in root, 3' from body 30" Elm tree (24')

△+40 30°-24' Right

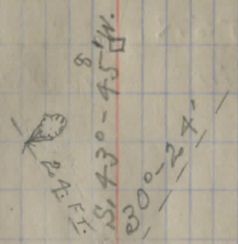
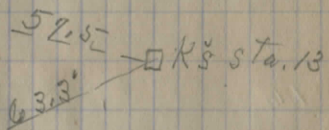
+12 2 nails in root 22" ash stump (29)
.10

2 tacks in 15" Hard Maple tree (35.3)

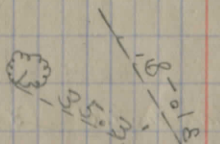
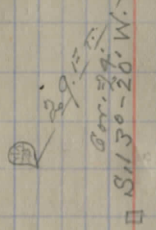
△9+40 31°-8' Left

9+33 2 Tacks in 20" white oak tree (9.0)

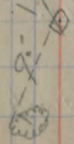
Outlet
Line Staked



Referenced



Referenced



10 12/8-1966 - Tiedler & Koenig (quit at 15-+15-)
Bass Lake ditch

16

+19 2 tacks in hard maple (7.0')

△+15 19°-56'R.

+12 2 tacks in hard maple (5.0')

15

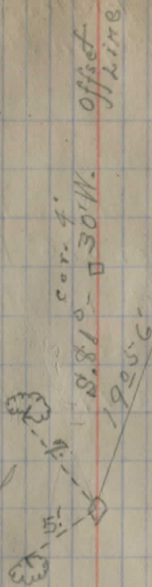
14

+08 2 tacks in 14" hard maple (34.0')

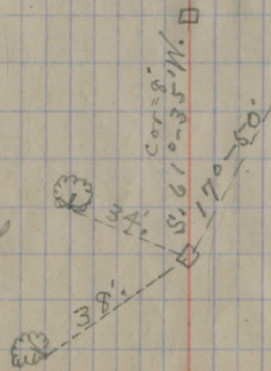
△ 13 17°-50' Right.

12+62 2 tacks in 10" Black Ash (38.0')

Referenced



Referenced



17 Bass Lake Ditch Fiedler & Pomaroy
12/11-1916

+30 Farm road across ditch
25 no stake (near pole foot bridge)

24+75 E ditch 12' to L. & old channel 12' to R.

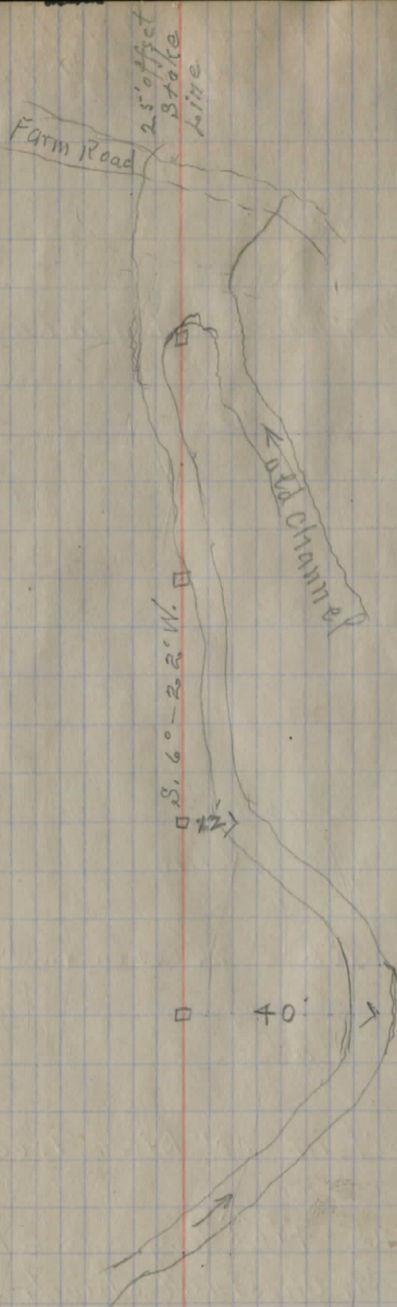
24 no stake - in stream near L. bank

23+74 stake on L. bank - 10' to & ditch to R.

23 22' to & ditch

22 40' to & ditch

21 no stake



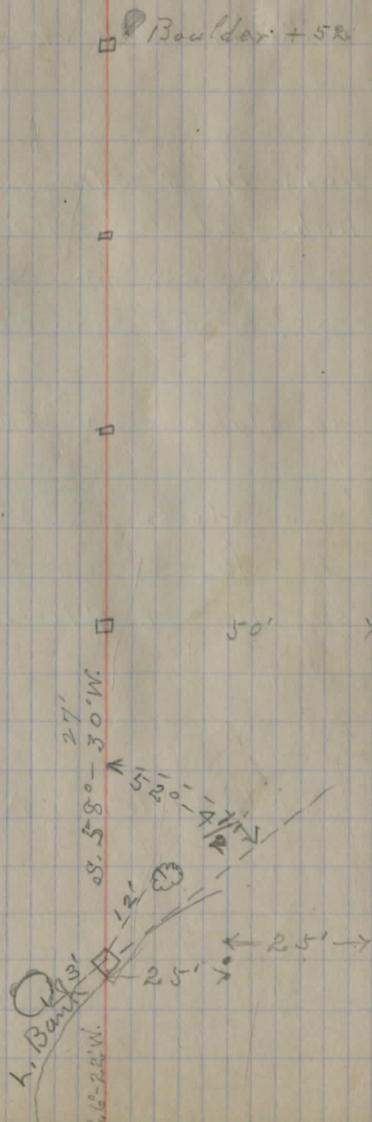
16 Bass Lake Ditto 12/11-1916
 Friedler & Pomroy

- 30 no stake
- 29 + 50 Hub. 7' to L. on Random Line
- 29 No Stake
- 28 + 50
- 28 no stake
- 27 + 50
- 27 no stake
- 65- Prop. by force of
- 26 + 50
 (Prop. line at 26 + 65 on random line)
- 26 no stake
- + 51 nail in 18" Birch Tree (12.0')
- 25 + 40 52° - 4' to 5' (Ang. calculated from Random Line)
- 25 + 36 2 ft. Chestnut stump - nail in root

Ref. Mansfield
 [Stakes set for fifty ft. offset line
 from 25 + 40 to 27 + 10]

Referenced

(6')



(Random line ang. 18° 29' 8'')

18 Fiedler & Bass Lake Ditch
Pomeroy 12/12-1916

35 in Ditch

+78.5 nail in root of 5" Elm 28.8'

34+57 nail in 8" Elm (9)

34+50 Hub (12' to ditch on L.)

" " " on Random line also, 2' to L.

34 no stake - in ditch ^{old} channel

33+50 no stake - in ditch ^{old} channel

33 no stake - in ditch ^{old} ✓

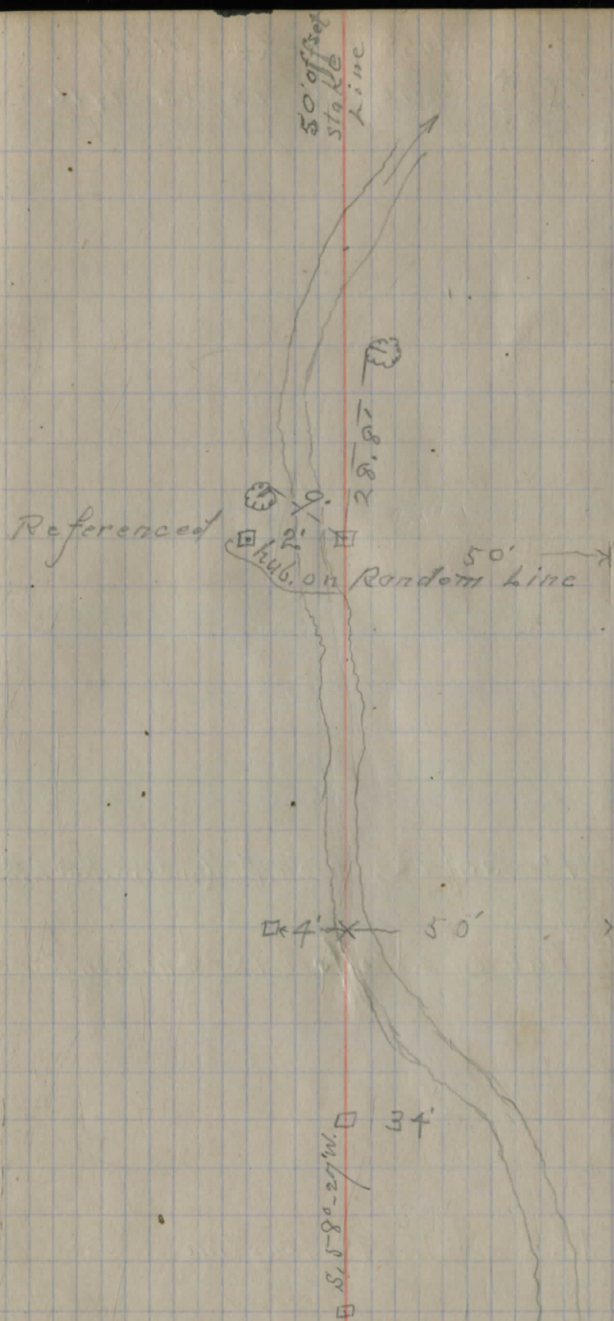
32+50 STAKE SET 4' to L. of Tangent Line

32

31+50 3+1/2' to ditch on R.

31

30+50



2.0 Bass Lake Ditch
 Fiedler & Pomeroy 12/13-1916

41

40

39

38

37+10 1°-30' - L. (27.4 to Random. Hub L. & 2.5' to 50' offset hub)

on 50' offset
 37+10 Hub on 2.5' offset R. - & hub on Random 0.6'

37

36+50

36

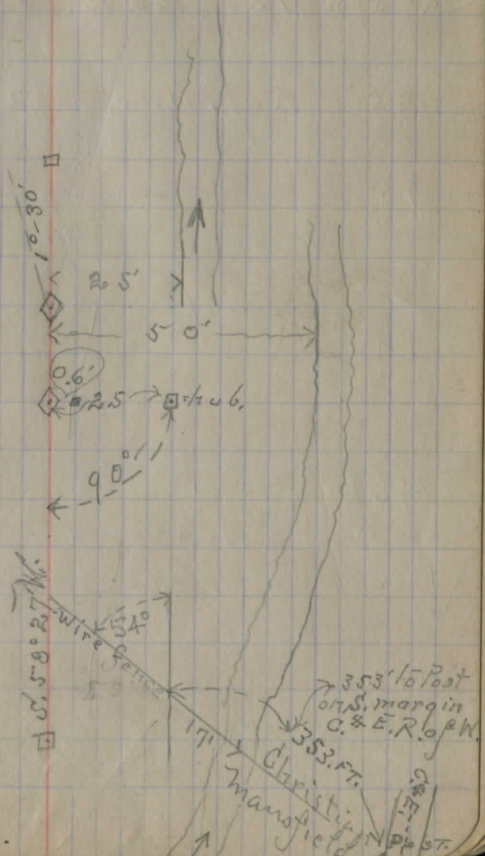
35+92 def. ang. to L. 54° = fence line

35+50

50.8
 25.0 offset
 57.8
 line

5' 56°-57' W
 0.8 5-9° W

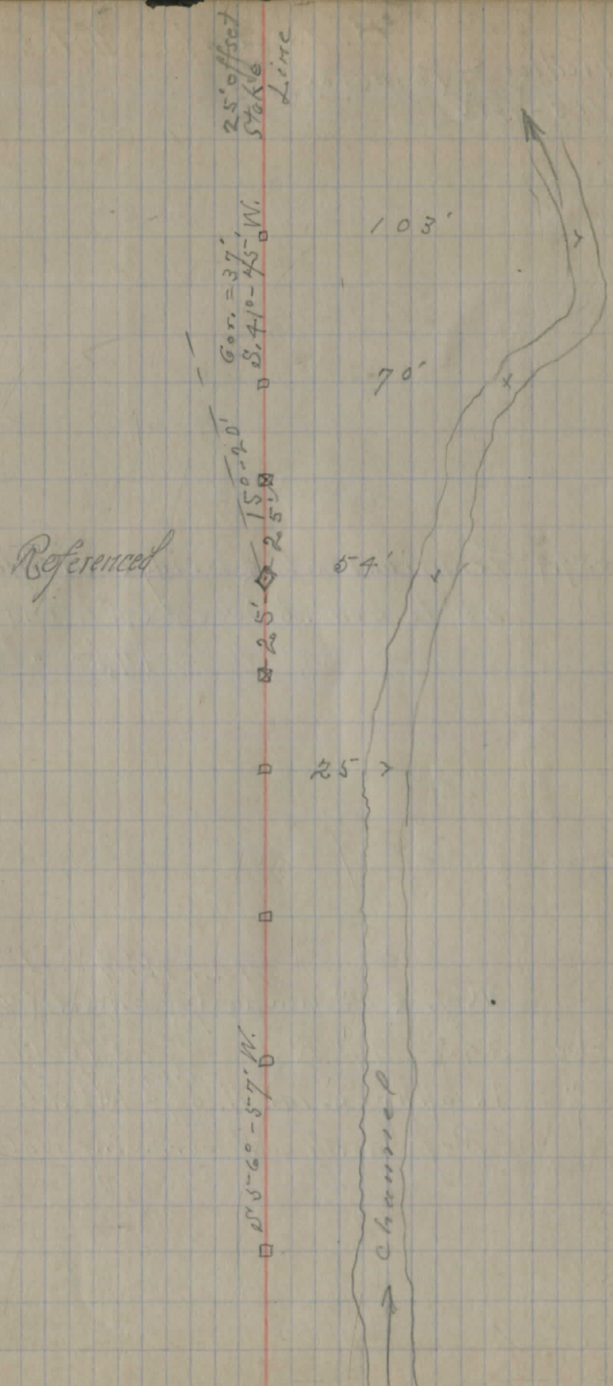
Referenced



East Lake Ditch

R.R. Fiedler & Pomeroy
12/13-1916
Sta.

- ✓ 47 103' to ditch channel
- ✓ + 50 curve to L. in old ditch
- ✓ 46 70' to ditch channel
- ✓ + 75 Ref. hub. (25') nail in top
- ± to be 21
△ 45+50 15'-20' h. 54' to channel
- ✓ 75 Ref. hub. (25') nail in top
- 45-
- 44
- 43
- 42



Cor. = 37°
S. 71° - 45' W.

150-20'
25.5

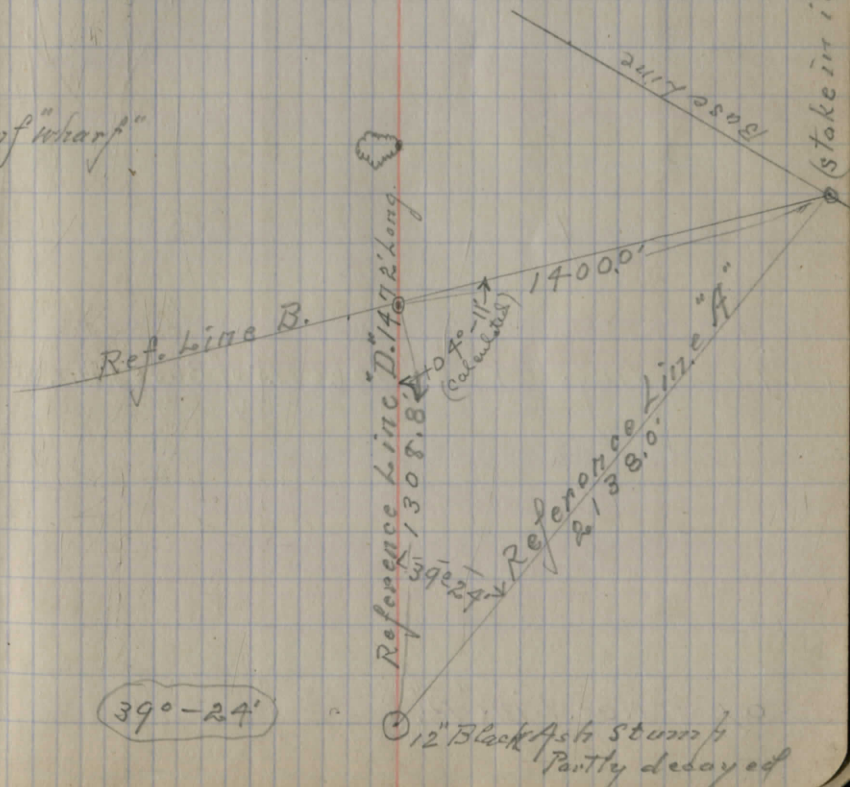
30 Bass Lake Vetch - Ref. measurements on ice
Jan. 25 - 1919 Middleton & P. Doloney - A.M. only

1472.0' spike in W. root 16" soft maple back

of "wharf"

1308.8' measured to Intersection of Line B.

0 = N. end Ref Line "A" (2138.0' Long)

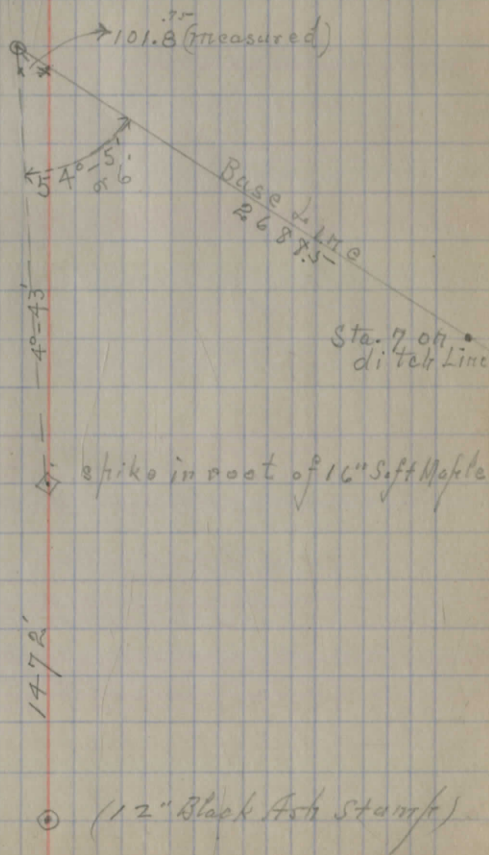


Fiedler & Kerrel 4/17th 1917
 Bass Lake Ditch

2688.5[△] of Base Line (stake) Ang. $54^{\circ} - 5$ or 6 min ^{5 1/2'}

147[△] R Ang. $\angle 4^{\circ} - 43'$ to 2688.5 of Base line

o of Ref. Line "D."



36 Bass Lake Witch
4/19-1917

Turning
R. from
V.B.S.
Fiedler inst
Keeney Rod-
Hainday "

360
272
118

Sta Rod N.S. Angles Elers Distances

15 Δ 6.46
5.08
3.70 5.1 242° 276 (setting 17)

○ 5.40
5.70
4.55 90

S 4 Δ 5.8
5.0
4.2 5.0 172° 37' 160

Lake ○ 12.8
11.2
9.6 5.0 72° 8' 320

+ 3 Δ 6.9
5.1
3.3 5.0 187° 36' 360

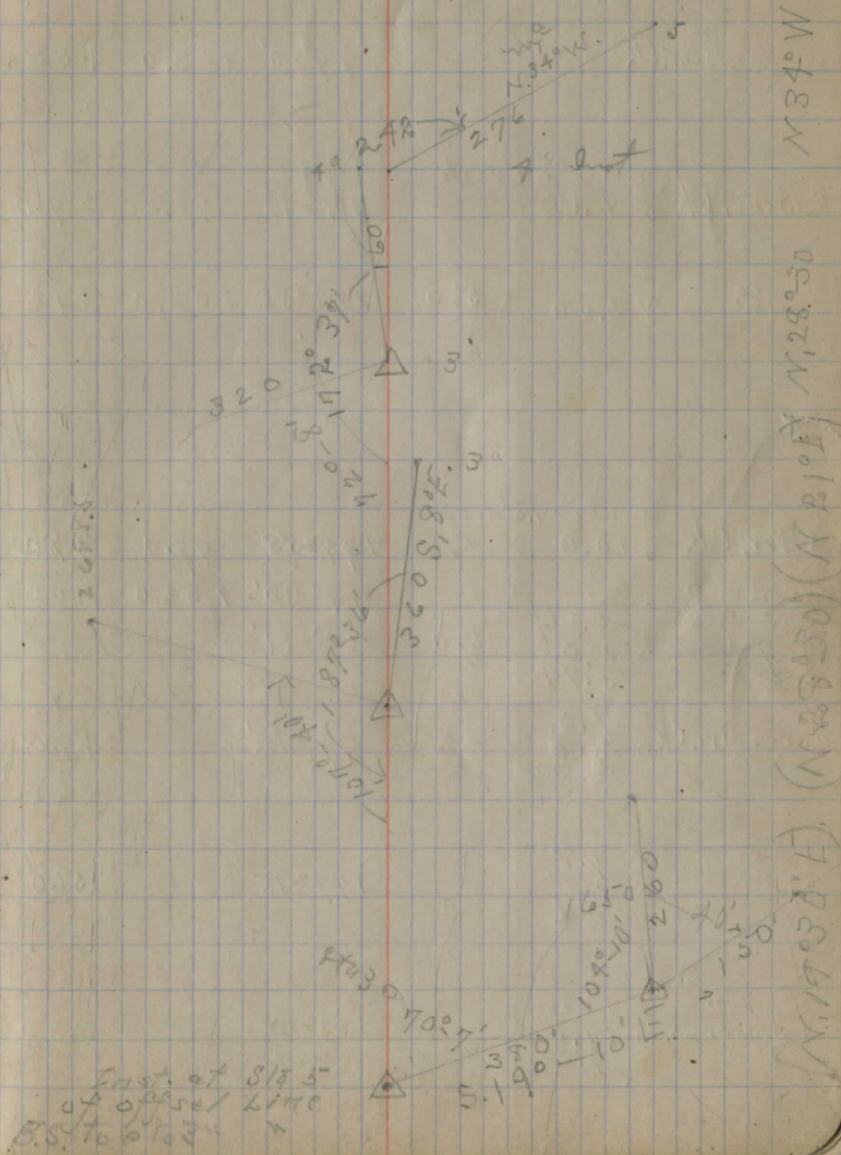
3 2 Δ 5.6
4.85
4.1 4.8 170° 8' 150

Prop. line ○ 5.20
4.80
4.40 165° 40' 80

Lake ○ 12.7
11.4
10.1 5.0 104° 10' 260

2 # 18 Δ 5.35
3.45
1.55 3.5 70° 7' 102. 380

(setting 17)



4/20-1917

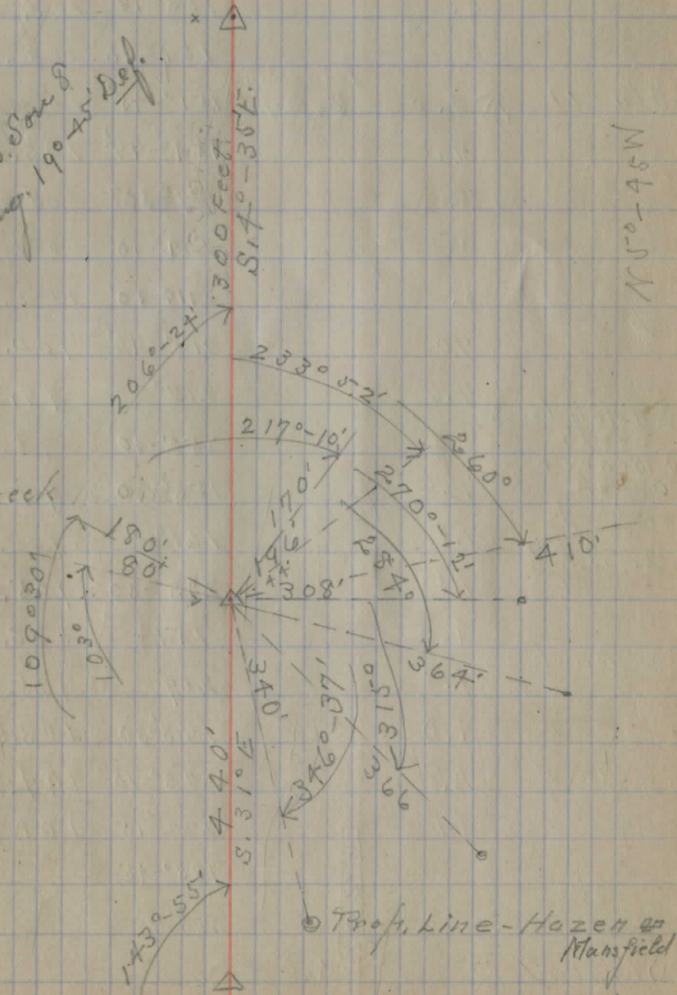
Foster
Downey
Keeney

Point	Red	H.S.	Angles	Elevs	Distance
a High water mark			142°		115'
Ber. ck	-5.0		342°	102.96	70
ditch to S.	-9.30		311-25	97.76	130'
B.M. "E"	+5.20	107.06		106.86	
Sta 10		57.0	206-24	102.0	300' ✓
2 Ber. ck	-9.2		283-20	97.86	38' ✓
Cent. of Bridge floor	-2.85		317-4	104.21	154' ✓
in road - Ribark			329-30		95' ✓
			238°		360' ✓
			260°		410' ✓
			109-30		180' ✓
B.M. "E"	+4.70	106.56		101.86	
			103°		80' ✓
			217-10		170' ✓
N. side Bridge	-9.1		233-52	97.96	196' ✓
			233-12		44' ✓
Sta X		4.5	143°-55'	102.	440' ✓
			270°-12'		305' ✓
			284°		364' ✓
			315°		366' ✓
			346°-37'		340' ✓

Sta 8

in return to
int. at 9 B. S. S.
Comp. ang. 190-45 Def.

2 Bearer Creek



N 50-45 W

4/20-1917

	Red H. J.	Angle	Elevs	Distance
Beaver Creek	6.4 Bottom		101.6	
	4. Bank	147°-20	104.0	540
	4.	157°-35	104.	460
	4.0	163°-40	104.0	440
	5.	171°	103	400 ✓
	5.	183°-15	103.	300-1
	5.	151°-30	103.	220 ✓
Sta 11	for readings 6.0 = 102	151°-45'	103.	550 ✓
	4.0.	157°-45'	103.0	600 ✓
	5.	> 187°-30'	102.0	700 ✓
	5.	> 202°-10	102	700 ✓
	5.	211°-30'	102.	600 ✓
Old	7.0	216°-40'	100.0	520 ✓
Old	7.6	212°-	99.4	420'
ditch to south	8.4	252°-30'	98.6	155 ✓
Beaver Creek on bank	7.6	153°-30	99.4	680 ✓
on bank	1.8	161°	105.2	730'
	1.5	203°-30	105.5	800
on bank	4.0	151°	103.0	580'
	1.3	209°	105.7	760
	4.0	143°-30	103.0	400
on Bank	2.8	223°-10	104.2	560
	4.1	222°-15	102.9	405.
		133°-45		220
		257°		185

Sta 10

102.0

50

△ #11

151°-45'

550'

△ #10

△ B.S. #9

4/20-1917

Fiedler
Romney
Recruit

Angle Elev Distance

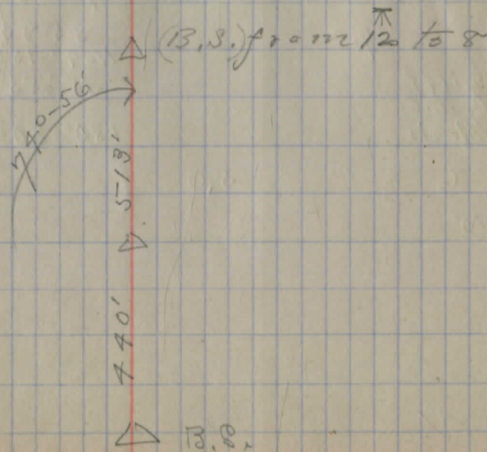
10' W. of
Hazen-Morris line

Angle	Elev	Distance
313°-26'		to Sta. #9
229°-15'	102	360
212°-10'	-	250'
255°-2'	-	365'
196°-10'	-	170'
276°-45'	-	340'
200°	-	80'
230°-30'	102	50'
191°	<u>103.20</u>	88'
74°-56'	-	513'

 BM "F" +3.38 5.50
 Sta 12 ^{B.S.} Δ

Sta 9 Δ

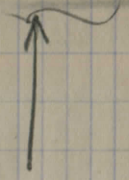
Sta 8 Δ



	Rod	H ₂ O	Angles	Elev.	Distance
Bottom	7.3		357°	99.3	150'
Bottom ditch	5.9		289°	100.7	25'
			212°-30'		70'
			236°-30'		150'
			253°-15'		260'
			267°-30'		360'
			290°-		350'
			308°-		320'
			324°-15'		280'
			350°-45'		190'
Sta 14 water 1.25 Lake	10.6	4.60	160°-17'	102	370'
			123°-10'	96.4	410'
			80°-5'		
water 1.25 Lake	10.6		85°-40'	96.4	390'
	7.0		85°-40'	100.	20' "
Sta 13		107.00 5.0	129°-55'	102	540'
	7.0		35°-53'	100.	10' -
			N. 4°-15' E		
			35°-53'	96.4	827'
Beaver Creek Outlet Property line Hazen Morris			170°-20'	102.	223'
Sta 6		5.0		102	
Sta 4					

Use 96.4 for low water mark - Till Stonecombs 22
B.M. is located

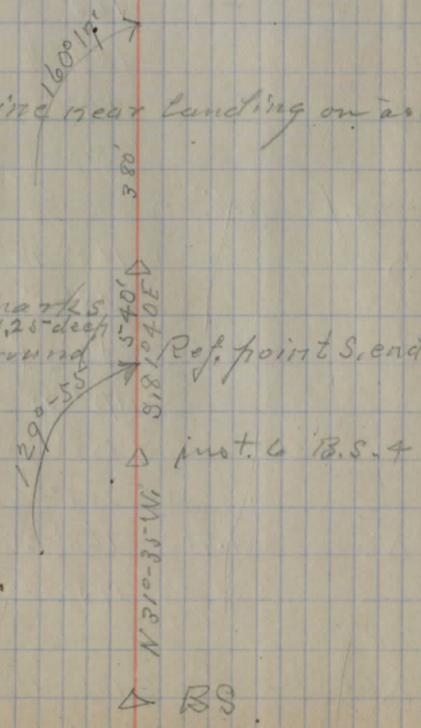
open ditch flow North
open ditch flow to N.



in meadow

N. end of Ref line near landing on ash stump

High water marks
water 1.25 deep
500 to hard ground
Ref. point S. end of line.



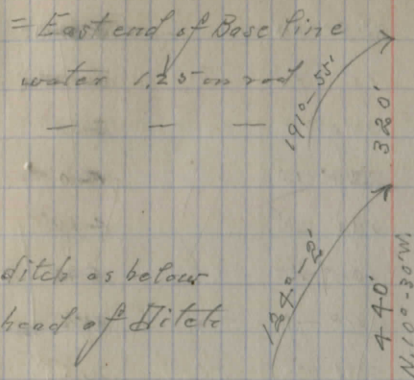
just 6 B.S. 4

BS

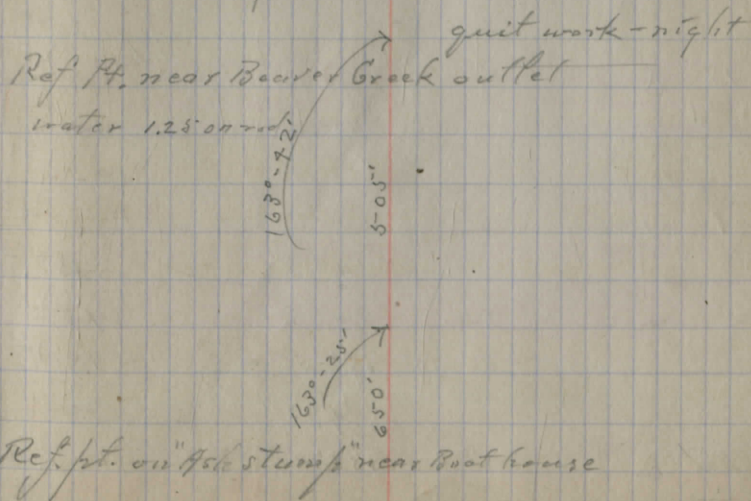
4-20-1917 + 4/21-1917
F. D. K.

Rod. H.9 Angles Elevation Distance

Sta.	Angle	Elevation	Distance
Sta 18.	191°-55'	320'	
Lake	131°-40'	260'	
Lake	102°-	300'	
Sta. 17 Δ	124°-2'	445'	
	108°-10'	410'	
	101°-20'	400'	
4.8	159°-30'	350'	
	138°-30'	325'	
	124°-40'	253'	
	110°-	180'	
	168°-5'	155'	
	129°-3'		
	49°-30'		
Lake	59°	460'	
B.M.	+3.25 (106.80)	103.55'	
Sta. 16 Δ	163°-42'	102.0	570.5'
	48°-5'		
Lake	57°-50'	293'	
	175°-35'	435'	
	188°-7'	325'	
	192°-10'	180'	
Sta 15 Δ	4.90	163°-25'	650'
		173°-40'	160'
		90°	100.00 30'
sta 14 Δ		106°-13'	



Prop. Line N. side Morris
ditch N. side Morris farm
Ref Pt. E. end Baseline
Ref. Pt. Beaver Creek
= 16' S. of prop. Line - Morris & -
Beech or Hickory



	Rod	H.S.	Angles	Elevations	Distances
Sta. 21			318°-34'		540'
Sta. 20'	Δ		251°-20'	102.00	160'
"			341°-20'		490'
"			63°-15'		41'
"			11°-45'		97'
Lake N.			250°-	96.4	235'
Lake S.			90°-	96.4	290'
			96°-15'		153'
			251°-35'		156'
			238°-45'		50'
Sta. 19	Δ		61°-53'	102.0	800'
			88°-		344'
			61°-50'		330'
Sta. 18	Δ				
{ B.S. on #1					
Sta. 1	X				
Lake			89°-5'		344'
			89°-5'		18.5'
		(N. 89°-30' W.)	89°-5'		
			69°-39'		
Sta. 18	Δ	57.3	338°-20'		106.
(B.S. 1517)					

(N.E. of base)

(Sta. 21 = inst at 19 - B.S. at 18)

(on N.E. Side of island)

± Road - Int. of tangents

± road small angle

± road

1.25' water

1.25' water on Road

= E. end of Base Line

1.25' water on rd

high water marks

Ref. sta 5 Base Line (on 25' offset stake line of ditch)

Ref. Pt. Deaver Creek

Intersec. of tangents of Bass Lake Road

4/21-1917

Ref	H.S.	Angles	Elevations	Distances
-----	------	--------	------------	-----------

193°-25' 440'

211°-30' 290'

200°-30' 366'

81°-21'

9°-0'

5/4, B.3	6.0	180°-40'	102.	480'
----------	-----	----------	------	------

143°-50' 280'

93°-45' 221'

340°-15' 190'

140°-15' 250'

Lake		67°-30'	96.5 ⁴	345'
------	--	---------	-------------------	------

B.M. Sta. 22	0.90	4.1	251°-30'	62'
--------------	------	-----	----------	-----

		154°-48'	102.0	530'
--	--	----------	-------	------

308°-15'

163°-45' 395'

193°-10' 520'

200°-30' 520'

190°- 430'

201°-30' 360'

199° 230'

289°-25' 57.5

96°-15' 60'

175°-30' 195'

Lake		65°-10'	96.7	171'
------	--	---------	------	------

Sta. 21		318°-34'	102.	
---------	--	----------	------	--

swail low till to NE

Subsided
Bidlake to
Barnstable
206.

Lake

Sta. 21

Ref pt. on "ash slump" w. of Boat house
E. end of Base line

ditch

Profile Bidlake

water 1.25 on Rod

B.M. Tree

Ref. pt. Beaver Creek

N. W. cor. Barn

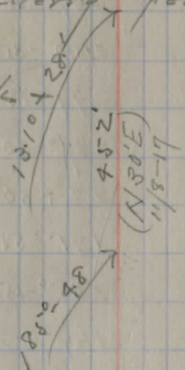
S. W. cor. of Ice house

130°-40'
450'157°-20'
530'

4/21-1917

Rod	#9	Angles	Elevation	Distances	
Sta 26	B.S. 25	293°-		210'	
		309°		110'	
		131°-28'	102.	452'	
		131°-20'		415'	
Sta 25	B.S. 24	85°-25'		540'	
		137°-25'		350'	
		137°-20'		185'	
		185°-48'	102.	620'	
		190°-15'		390'	
		187°-50'		265'	
		184°-45'		190'	
Lake bottom	S	159°-30'		65'	
		63°-35'	96.4	570'	
		192°-45'		195'	
		212°-40'		230'	
		236°-30'		100'	
		262°-		95'	
		215°-45'		63'	
		184°-40'		100'	
		62°-2'			
		344°-35'		386'	
Sta 24	B.S. 23	5.0	186°-28'	102.	652'
Lake	B.S. 22		106°-		370'
Sta 23					

on Edwards Cherry point-

Prop. line Hanslick
Edwards

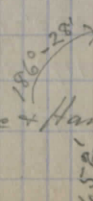
Lake Pine

1.25 water on road

620'

To Ash stump on Ref line
Bidlake & Hanslick line

Prop. line Bidlake & Hanslick



4/21-1917

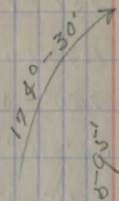
Reel	H ₂	Angles	Elevs.	Hist.
Sta. 29 "A"	○	208°-5'		280
Sta 29	△	174°-30'	102.00	595'
		269°-30'		290'
		280°-30'		210'
		297°-15'		150'
		289°-30'		90'
		224°-30'		100'
		191°-55'		300'
		125°-15'		480'
Sta 28	△	169°-12'	102.00	375'
		166°-35'		280'
		169°-0'		200'
		74°-45'		
Sta 27	△	187°-43'	102.00	281'
		183°-20'		150'
		111°-0'		560'
		87°-25'		
		194°-10'		140'
		218°-40'		235'
		233°-15'		380'
		238°-30'		220'
		220°-10'		55'
		119°-30'		165'
		243°		350'
		269°-10'		310'

Sta 26

B.S. 25

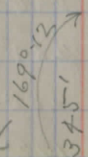
(Located from 28 & B.S. 27)

(to finish swamp)



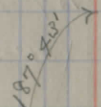
nail in green ash stump N. end Ref Line

Ref. pt. on ash stump



check this

to Ref. pt. ash stump



281'

outlet of tile into of pond at 6

	Red	H.S.	Angles	Elevs.	Distances	
			153°		180'	
Sta. 30	Δ	4.9	151°-44'	102.0	580	across inlet ditch
			189°-50'		520'	across inlet ditch
			180°-50'		460'	across inlet ditch
			56°-20'		780'	ang. in ditch + near mouth of inlet
			65°-5'		620'	ang. in ditch
			158°-50'		292'	ang. in ditch
		9.0		98.0		water in inlet approx. 10'
			229°-44'		645'	inlet ditch at ang. pt. Brook from N.W. 30' above this
			240°-50'		225'	
			234°-0'		390'	
			202°-50'		206	
			192°-50'		200'	
			159°-20'		120'	point of high ground s. of inlet ditch
Sta. 29	Δ	6.15	51°-50'		460'	N end of Ref. line nail in stump
		5.3		101.7		water in swamp
			268°-30'		175'	
			229°-45'		320'	
			275°-30'		80'	outlet to swamp easterly side
			286°		94'	outlet to swamp - westerly side
			237°		390'	
			260°-40'		350'	
		8.70		98.3		water at outlet same
{ Sta. 29 "A"	○	5.0	122°-50'	102.	391'	check on Sta. 29
{ B.S. on 28						

Sta	Red	H. O.	Angles	Elevs.	Distances
Sta 36	△		181°-21'		290'
Culvert G & E	38		196°	103.00	140'
			252°		39'
			177°-		142'
			197°-		65'
Sta 35	△		179°-28'		212'
			265°		58'
			177°		110'
Sta 34	△		129°-46'		320'
			100°		84'
nail in Py Tie			283°-40'		340'
			229°		95'
			250°		110'
			250°		125'
18" Py Culvert	5.2			101.6	
			328°-		120'
			287°-0		62'
			2°		100'
Sta 33	△	4.8	171°-8'	102.	320'
			111°		5'
			191°		184'
			163°-30'		100'
			149°-27'		360'
			149°-30'		298'
Sta 31	△				
Sta 30	△				

B.S. 34

B.S. 33

B.S. 32

B.S. 31

B.S. 30

B.S. 29

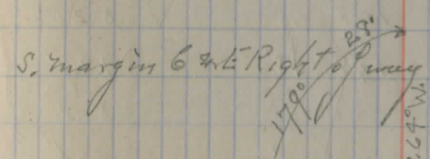
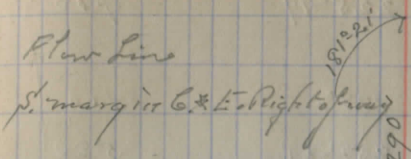
B.S. 28

B.S. 27

B.S. 26

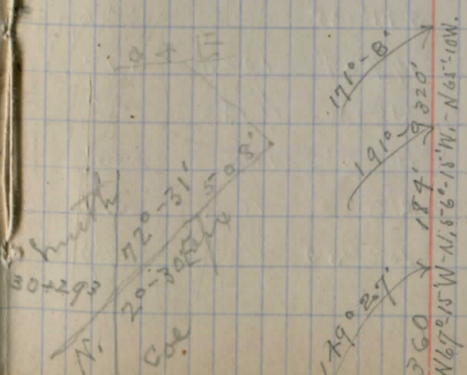
B.S. 25

o/kansila



Bass Lake Survey - Random line - N side Bass Lake Property

flow line water 0.75' deep



(5' E. of 12" bench)

305' to station

Sta	Rel	H.D.	Angles	Elev.	Distances
Sta 43			225°-19'		400'
			128°-		100'
42 Sta.			251°-24'		580'
			198°-45'		520'
			198°-45'		429'
Sta 41			129°-25'		335'
Sta 39					
Sta. 40			192°-41'		353'
Sta 39		6.7	117°-11'	100.3	283'
			206°-		170'
			177°-		60'
			341°-25'		326'
Sta 38		5.0	179°-34'	102.0	312'
		4.55	246°-30'	103.45	72'
Sta 39		5.0	158°-19'	103.	263'
			260°-	102.	3.5'
			156°-30'	102.	220'
Sta 36					

Iron pipe set
near gravel & sand beach, S. of clump of Soft Maples.

shore line

near shore line - Iron pipe set (S. 1° W.)

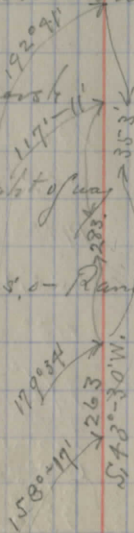
Shore line of Lake Outer fringe of bushes,
near shore line & across "Burnt area."

Tack in tie 4" No. 8 Nail on Random Survey Line

out in cranberry marsh

margin of C & E Right of way

Int. of C & E Ry. Tang. to Random of Survey
quit on 38



7/24-1917 F. W. S. R.

Rod H. J. Angles Elevations Distances

	Angles	Elevations	Distances
<u>Quation ash stump</u>	42°-58'	216.5'	204'
Sta 46 Δ	25°-6'-7'		371'
B.S. on 44			
Sta 45 Δ	97°-49'	209'	
B.S. 43	162°-39'	166'	
Sta 47 Δ	238°-19'	280'	
		<u>99.60</u>	
1.6		104.5'	
	146°-22'		546'
	142°-		375'
	178°-53'		
	130°-45'	102.	260'
	116°-		174'
Lake surface 9.6	71°	96.4'	135'
44 Sta Δ all above	106.05'	238.14'	270'
B.S. 42	142°-16'		
	153°-5'		
	213°		275'
	200°		195'
	161°		125'
	122°-0'		70'
Sta 43 Δ	212°-32'		

To Beaver Creek end of Ref. line
to Sta. 45
B.S. to Ref. line across Lake to pt. at Maple Tree

across Track of C.R.R.

To Ref. pt. on ash stump

Bet. Boat House & Track E. of path

on knoll

See Page 70

water Surface 4/24-1917

Highest pt on "knoll"

N. cor. of boat house

Cor. Post of Lot Cor. back of Old Cottages (for checking)

shore line

shore line 112.5' ^{water} on road

on knoll

Ref. pt. on Island - Maple tree - nail in Rod

" " at Beaver Creek

See above

Ref. pt. ash stump

40

✓ 161° 20'	645'
✓ 158°	475'
✓ 156°	430'
✓ 155°	330'
✓ 148°	215'
✓ 132° -	125'
✓ 90° -	60'
✓ 82° 30'	160'
315° - 50'	515'
	280'

s/s 45 -
46 B.S. 46

Dist. on Track G. & E. N. rail B.S. on 46 # Ang 10'

153° - 30'	340'
118° 40'	485'
✓ 156° - 40'	230'
✓ 154° - 20'	260'
✓ 150° - 30'	215'
	245'
	185'
✓ 126° -	96'
✓ 115° -	357'
✓ 115° -	63'
✓ 69° - 20'	370'
✓ 64° -	180'
✓ 18° - 45'	75'
- 304° -	95'

Ash. Stump (B.S. to Maple tree joint across lake)
End of Ref. line D

s/s Sta no. 40 on G. & E.

s/s 40 -

Sta 40 = 161° - 20 distant 645 FT. (280' to 46)
(offset line - rail in tie G. & E. + Bass Lake Survey)

? check for above

at G. & E. Ry
Spring BrookShore line & mouth of cold Spring Brook
N. end of Ref. line has stump

Red HD Angles Efers. Distance

Sta 50
 236° 240'
 175° 42'
 175°- 110'
 127°-30 160
 117°-30 302'

Sta. 49
 136° 307'
 121° 270'
 110° 240'
 88° 210

Sta 48
 180° 296'
 138°- 230°

Sta 47
 180° 410'

150° 102. 110'
 180° 710'
 173° 102 240'
 164° - 200'
 150° - 165'
 131° - 155'
 111°-12' 102. 165'

BS 49

BS 48

BS 40

BS 40

8.70

110.70

9.90

111.90

Inst. on tack of offset line x G&E. in tie & B.S. 15

shun line
 prop. line
 shun line
 & here line

70, 50 near lake

(S. 3°-20'E)

on Ry

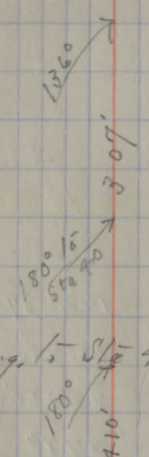
tack in tie, Tang. to Sta 40

Tack in tie on Tang. for #47
 & stem and near knary in G&E right of way

Prop. line Bass lake & Hazen

Efers. peg.

N. Ending G & E line x



4/24-1919

Prod. H.S. Angles & Distances

Sta 45	Δ	✓ 162°-39'	65'
		✓ 72°-20'	70' ✓
		278°	100' ✓
		285°	138' ✓
		305°	125' ✓
		325°	135' ✓
		(0,0)	130' ✓
		360°	70' ✓
		350°	
		335°	

P.S. 43

Sta 44

Δ

setting 45 - near path → 1st Stop on Ry (S. 88° - W.)

Ref pt. on island across Lake

162°-39'

664 feet

Smith's "Island Knoll" (See Page 64)

Red H.D. Angles Elev. Distances

Sta.	H.D.	Angles	Elev.	Distances
S/a. 1		195°		260'
		141°-		200'
		300°-		140'
		146°-		100'
		195°-		26'
S/a. 5-4	B.S. 53	113°-44'	24	383'
		24	conform to	moving stake
S/a. 5-3	B.S. 51	198°-10		206'
		108°-		235'
		110°-		195'
		95°-		95'
		182°-20		283'
S/a. 5-2	B.S. 49	165°	102.	182'
		159°-		215'
		173°-		100'
		209°-		91'
		233°-	102.	65'
		207°-12		240.
		216°-		145'
257°-		100'		
S/a. 49	B.S. 48	219°-		75'
		156°-		125'
		342°-		140'
		5:00	102.00	

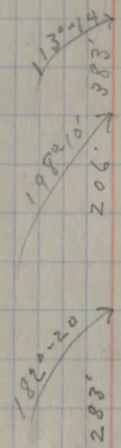
is sta. 5 of offset stake on ditch

down stream
up stream
old channel P

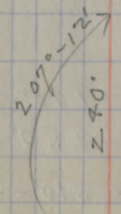
N. 22°-15' W.

N. 44°-30' E. Rain

stream as below



stream



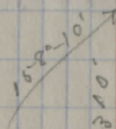
B.S. 55-
 25 2/5
 195° 150'
 280° 70'
 118°-10' 310'

B.S. Sta. 12/5
 ori. on Base
 190° 180'
 250° 110'
 310° 380'

Sta. 1 A 262°-11 1/2 Sta. 54

← hills

N. 19° E approx



shore line
 1/2 Shore line

Beyond old Crummett

water in 5-011

310° (B.S. as below)

B.S. on Sta. 3 of offset stake line for ditch

4/25-1917-

Rad	H J	Angle	Colors	Distances
-----	-----	-------	--------	-----------

159° 730'

152° 390'

148° 325'

210'

167°-48' 220'

165° 260'

168° 280'

156° 250'

180° 341'

140° 270'

149° 250'

152°- 220'

157°- 170'

160°- 185'

132° 220'

120° 195'

101° 115'

68°-80' 145'

43° 150'

20°- 220'

13°-30' 215'

357°-45' 185'

346°-20' 290'

342°-12' 400'

cent 20' Knoll

to look in tie near W. prop line Base L. Gun (Tangent)

banks of brook

S. of Track

Lid. on Track C. & E.

B.S. Bent Hughes & Son, End of Ref. Line at Maple

Sta W.

2000

105'

East

Sta X.

123°

78'

South

170°

40'

South

Sta W.

245°

156'

West

264°

8f'

West

Int.

820

100°-25'

210'

East

420

11/8-17

93°-25'

N. 80° E

25'

S. 73° E

73°

S. 15° E

N 11/2° E

End of Ref. Line

82 Bass Lake Ditch
W. of N. + S. Center Road

58+60.5 $\Delta = 44^{\circ}25' L$

44-25
88-50

56+80.0 $\Delta = 42^{\circ}29' R.$

42-29
84-58

51+08.5 $\Delta = 46^{\circ}00' L$

46-00
92-00

49+57.4 $\Delta = 9^{\circ}09' R.$

9-09
18-18

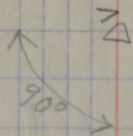
Feb. 4, 1928
Thaw - Mist.

W.C. Marks
Harvey Goodrich
Harry Klaus

40

Fence
~~XX~~

262'



50'

Δ

< 25'

Δ

< 25'

Δ

Proposed Δ of Improvement

72+15

68+18.3

$\Delta = 10^{\circ}10' R$

100/0
200/21

64+70.5

64+50.0

0°00'

62+31.2

$\Delta = 27^{\circ}52' R$

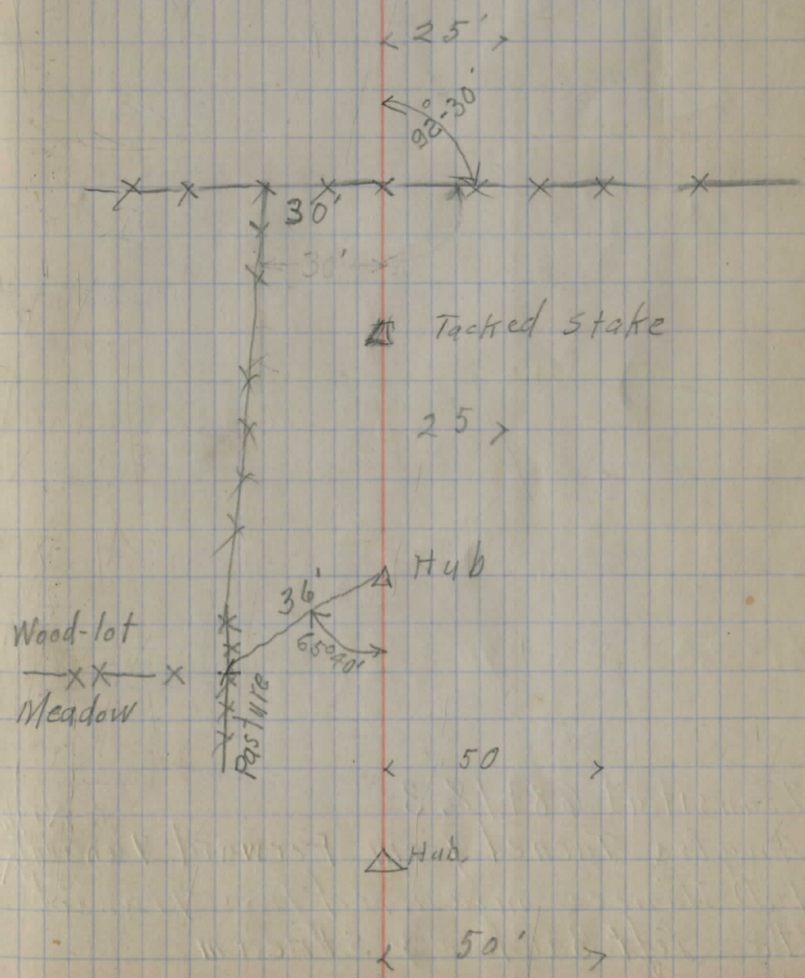
27-52
55-45

60+59.8

$\Delta = 27^{\circ}22' R$

27-22
54-44

top of old Dam



76

Transit at 68+18.3
 Angles Turned from Forward Tangent ^{to Right}
 + Distances measured from Transit
 to left Bank of stream

42

24-30	102	25
49-00	100	15
90-00	103	25
98-55	127	28
106-45	139	20
111-05	125	30
104-25	110	20
98-35	93	20
96-45	55	20
104-00	45	25
128-35	44	20
Angle	Dist.	Width of stream

81+79.5

77+02.0 $\Delta = 40^{\circ}58'$ Left
stopped, Feb. 4, 1928

74+00 $\Delta = 24^{\circ}43'$ L

$40^{\circ}58'$
 $81^{\circ}55'$

24-03
49-26

Willow
E. W. FENCE
H46
< 25' >

Δ H46

< 25' >

6.80 1148.37 1141.57

5.70 1142.67

1144.06

97.15

97.24

97

Feb. 8, 1928 P.M. Marks + Clause

Showers

44

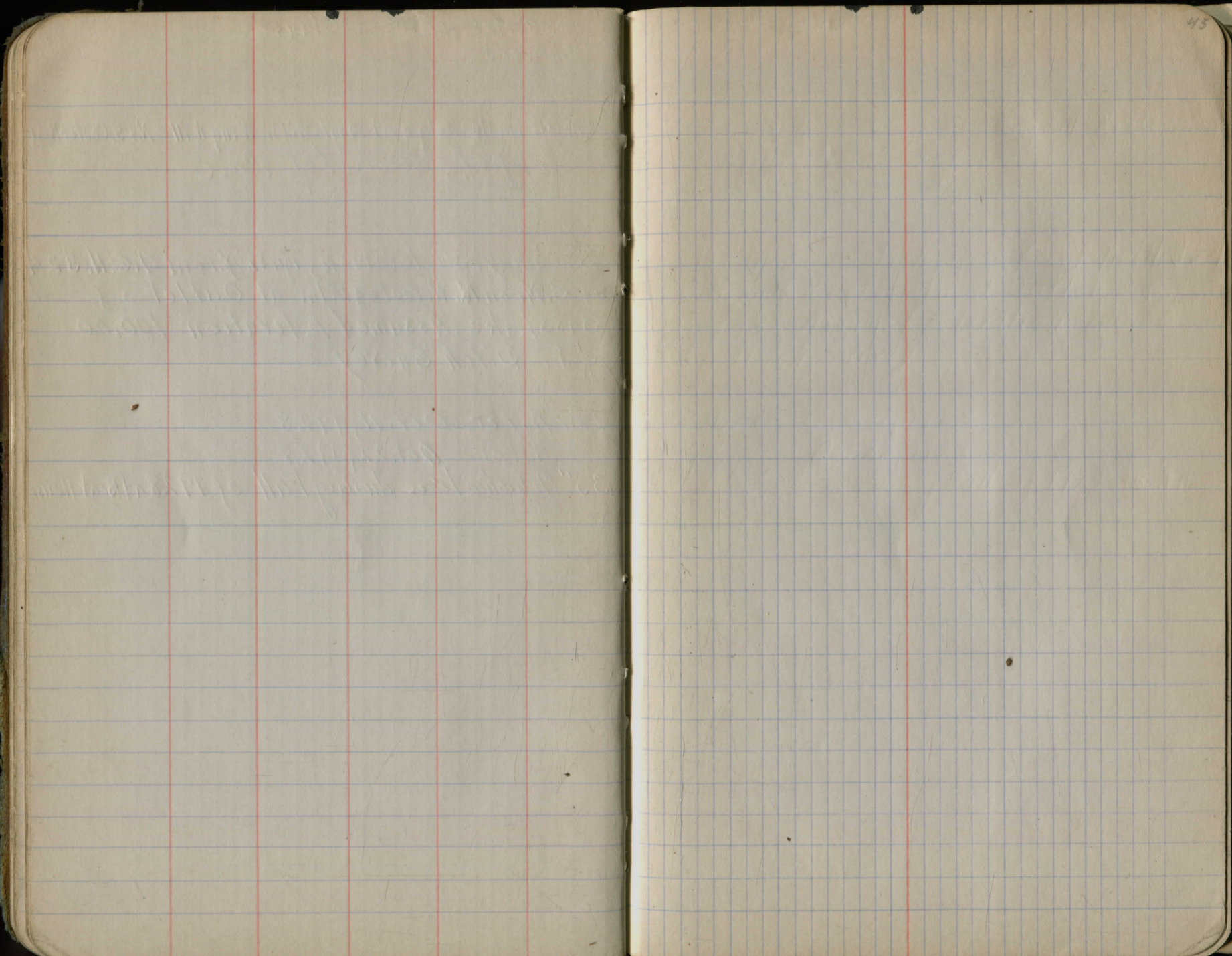
B.M., NW Wall Bridge at Angle with Wing Wall - N + S, Center Road
stopped, account of Rain

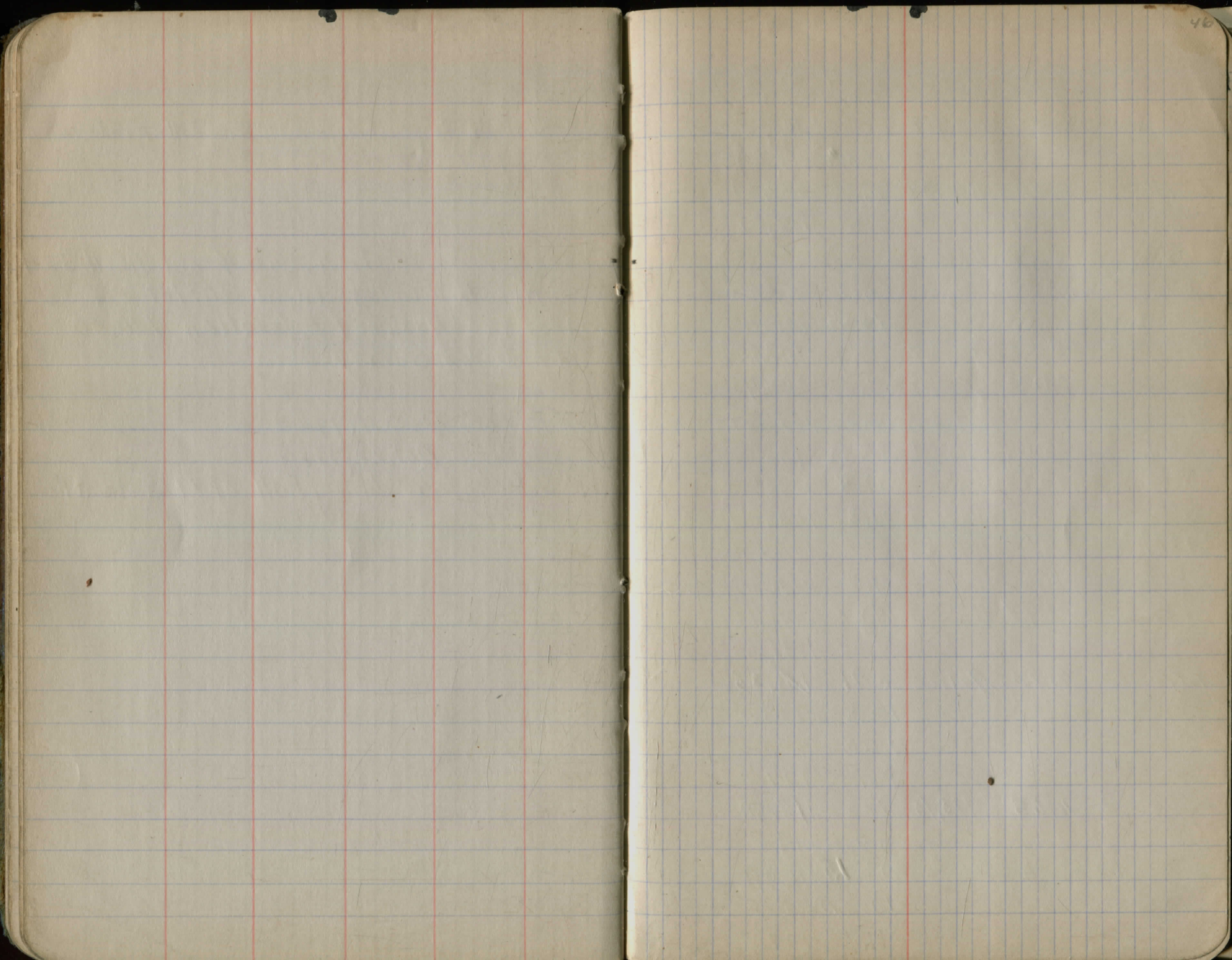
Zethmayr's Elevation, run from I.C.H. 324
of B.M. on N.W. root of Elm at Outlet of
Bass Lake, Assumed Elevation 100.00
of Ditch Survey

Low Water, Oct. 11, 1928

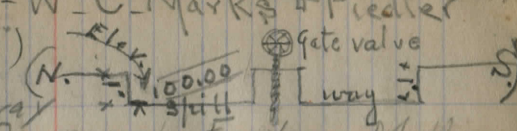
Water Oct. 22, 1928

33" Fluctuation during Fall of 1928 at Boat House





	+ R.	H.S.	- R.	Elev.
	269	107.69		100.00
			8.4	97.3
T.P.	6.90	114.59	0.00	107.69
T.P.			6.17	108.42
T.P.	4.41	112.83		
			16.4	96.4
			12.4	100.4
T.P.	3.85	112.27	4.41	108.42
T.P.	6.04	114.73	3.58	108.69
			6.3	108.4
			15.4	99.3
			11.4	103.3
			11.3	103.4
			9.1	105.6
			11.0	103.7
			14.0	100.7
			5.0	109.7
T.P.	7.70	121.52	0.91	113.82
			13.5	108.0
			16.5	105.0
			11.4	111.1
	6.65	125.15	3.02	118.50
			10.6	114.6
			14.25	111.00
			10.00	115.15
			17.7	109.5

Dec. 17, 1927 - W.C. Marks & Fiedler
 (Wm Miller's Inspector) 

Assumed E.L. of Dam at Fowler's Mills
 Water level of Pond (+ from gate valve in dam)

Stream Bed, Jones-Russell West Line
 High Water Level

Top of Dam " " Property
 Stream Bed ^{at dam} " " " "
 Top of Water ^{at dam} " " " "
 E.L. of Culv. across C. & E. - R. & W.
 N. End of Rail of Foot-Bridge
 Low Point in cultivated Field N. of stream
 Stream Bed at Foot Bridge
 Drive-way across C. & E. - Russell & Jones
 Water Level Miller-Jones-Russell Line
 Bed of Stream
 " " " Ry. culvert 50' E. (Russell)
 " " " Rd. culvert w. of Mansfield vi.
 Water surface, N. & S. center Road
 Top of curb
 Stream Bed

	BS	HI	FS	Elev
B.M.				1141.57
B.M.	2.08	1186.38		1184.30
T.P.	0.32	1171.09	15.61	1170.77
T.P.	0.40	1155.25	16.24	1154.85
T.P.	3.14	1145.66	12.73	1142.52
B.M.			4.23	1141.43
BM	4.23	1145.80		1141.57
T.P.	9.91	1146.69	9.02	1136.78
BM	5.21	1144.51	7.39	1139.30
TP	3.78	1138.62	9.67	1134.84
TP	3.04	1137.45	4.21	1134.41
BM	9.22	1140.28	6.39	1131.06
TP	7.80	1147.97	0.11	1140.17
TP	1.77	1148.87	0.87	1147.10
BM			7.29	1141.58

X on W. Wall of Bridge, S. End.

S. E. Root of Hickory opposite Miller's House

1141.57 Rec. X on West Wall of Bridge at Angle with ^{S.W. Wing-Wall}

top Stake 54+00

N root 18" Elm Sta 62+70 and 75' L of traverse line

top Hub Sta. 68+18.3

N root 30" maple Sta 74+70 and 45' L traverse line

Sta	BS	HI	FS	Elev
BM	0.88	114245		1141.57

Sta 50

Sta 51

Sta 52

Sta 53

TP ^{Top Stake 54} 5.12 1141.90 5.67 1136.78

Sta 54

Sta 55

Sta 56

Sta 57

TP ^{Hand (50)} ₅₆₊₄₆ 7.44 1144.99 4.35 1137.55

Sta 58

Sta 58+60 Section at $\frac{1}{2}$ (bisecting Angle)

TP ⁵⁸⁺⁶⁰ _{top of 11} 2.70 1146.17 1.52 1143.47

Sta 59

X on W wall bridge S End

1137.8	1137.3	1134.9	1133.8	1135.3	1136.7	1136.7		
4.7	5.2	7.6	8.2	7.2	5.8	5.8		
<u>0+00</u>	<u>3.00</u>	<u>9.0</u>	<u>22.0</u>	<u>32.0</u>	<u>39.0</u>	<u>5.0</u>		
1137.0	1137.1	1135.8	1134.7	1134.2	1134.3	1135.8		
5.5	5.4	6.7	7.8	8.4	8.2	6.7		
<u>0</u>	<u>1.4</u>	<u>1.6</u>	<u>1.8</u>	<u>2.5</u>	<u>3.2</u>	<u>3.4</u>		
1136.3	1136.4	1133.9	1134.2	1136.1	1136.9	1136.8		
6.2	6.1	8.6	7.3	6.4	5.6	5.7		
<u>0</u>	<u>1.8</u>	<u>2.0</u>	<u>2.9</u>	<u>3.3</u>	<u>4.2</u>	<u>5.8</u>		
1136.7	1136.1	1134.1	1134.0	1135.3	1135.8	1136.7		
5.8	6.4	8.4	8.5	7.2	6.7	5.8		
<u>0</u>	<u>2.6</u>	<u>2.3</u>	<u>3.2</u>	<u>3.4</u>	<u>4.9</u>	<u>7.0</u>		
1136.0	1136.0	1135.7	1135.1	1135.1	1133.8	1134.1	1136.2	1136.3
5.9	5.9	6.2	6.8	6.8	8.1	7.8	5.7	5.6
<u>0</u>	<u>1.4</u>	<u>2.4</u>	<u>2.5</u>	<u>3.1</u>	<u>3.2</u>	<u>3.3</u>	<u>4.2</u>	<u>6.6</u>
1136.3	1136.3	1135.0	1134.0	1133.4	1133.4	1135.6	1136.1	1136.3
5.6	5.6	6.9	7.9	8.5	8.5	6.3	5.8	5.6
<u>0</u>	<u>1.0</u>	<u>1.5</u>	<u>1.7</u>	<u>2.0</u>	<u>2.5</u>	<u>2.9</u>	<u>4.5</u>	<u>5.9-15.0</u>
1136.6	1135.6	1133.4	1133.4	1135.3	1135.5	1136.2		
5.3	6.3	8.5	8.5	6.6	6.4	5.7		
<u>0</u>	<u>1.1</u>	<u>1.3</u>	<u>2.5</u>	<u>2.9</u>	<u>3.3</u>	<u>4.3-20.0</u>		
1137.1	1136.5	1133.6	1133.7	1133.6	1134.6	1135.2	1135.4	1136.0
4.8	5.4	8.3	8.2	5.3	7.3	6.7	6.5	5.9
<u>0</u>	<u>1.0</u>	<u>1.3</u>	<u>2.1</u>	<u>2.3</u>	<u>2.7</u>	<u>3.9</u>	<u>5.7</u>	<u>4.1-20.0</u>
1142.4	1140.6	1137.8	1135.7	1134.7	1133.6	1133.6	1135.9	
2.6	4.4	7.2	9.3	10.3	11.4	9.1		
<u>0</u>	<u>1.3</u>	<u>1.9</u>	<u>3.9</u>	<u>4.3</u>	<u>4.6-5.6</u>	<u>6.7-26.0</u>		
1143.2	1142.0	1137.6	1136.2	1135.8	1133.5	1134.5	1135.5	
1.8	3.0	7.4	8.8	9.2	11.5	10.5	9.5	
<u>0.0</u>	<u>1.2</u>	<u>1.7</u>	<u>2.6</u>	<u>4.5</u>	<u>5.1-6.0</u>	<u>6.2</u>	<u>7.0-level</u>	
1143.8	1142.8	1137.9	1135.3	1134.4	1133.7	1133.4	1134.4	1135.6
2.4	3.4	8.3	10.9	11.8	12.6	12.8	11.8	10.6
<u>0</u>	<u>1.0</u>	<u>1.6</u>	<u>3.4</u>	<u>4.0</u>	<u>4.3-4.9</u>	<u>5.4</u>	<u>6.2</u>	<u>7.0</u>

Fence

	BS	HI	FS	Elcv.
		1146.17		
TP	1.98		2.70	1143.47
60.				

T.P.	0.80	1144.27		1143.47
------	------	---------	--	---------

60+59.8

61+00

61+75

62+00

BM	2.67	1141.96	4.98	1139.29
----	------	---------	------	---------

62+31.2

63+00

63+25

64+00

64+50

Top	4.01	1139.63	6.39	1135.62
-----	------	---------	------	---------

1143.5	1142.7	1135.3	1135.3	1133.9	1135.7
2.7	3.5	10.9	10.9	12.3	10.5
0.0	1.9	3.2	4.1	5.3	6.8-2.06

Feb. 13, 1928 Clear, 22° Marks - Goodrich
Clause - Rand

Top of Hub. 58+60

1140.5	1141.1	1138.7	1134.3	1133.1	1132.6	1132.7	1134.2	1134.6
3.8	3.2	5.6	1.0	11.2	11.7	11.6	10.1	9.7
00	2.6	3.2	3.6	4.0	4.4	4.9	5.4	6.5
1140.1	1141.1	1138.9	1133.1	1133.1	1133.7	1134.2	1134.5	
9.2	3.2	5.4	11.2	11.2	10.6	10.1	10.8	
0.0	2.1	2.8	3.8	4.3	4.8	6.1	8.0	
1137.6	1138.5	1139.4	1139.6	1134.3	1133.3	1132.7	1132.5	1134.3
6.7	5.8	4.9	4.7	10.0	11.0	11.6	11.8	11.7
0.0	1.2	1.7	2.6	3.2	3.6	3.9	5.6	6.1
1136.1	1134.6	1132.9	1132.5	1132.7	1134.4			
8.2	9.4	11.6	11.8	11.0	9.9			
0.0	3.1	3.6	4.9	5.4	6.5			

1139.30 rec. N. Root 18° E / m 75° L. of 62+70

1138.7	1138.4	1134.5	1133.7	1132.7	1132.6	1133.8	1135.2
3.3	3.6	7.5	8.3	7.3	9.4	9.0	6.8
0.0	1.2	2.1	2.9	3.3	4.3	4.7	5.6
1137.7	1133.3	1132.9	1132.8	1133.3	1133.2	1135.7	
5.3	8.7	9.1	9.2	8.7	8.8	6.3	
10.0	5	0.0	8	16	3.6	5.3-8.0	

Small Stream enters from Left

1140.1	1135.8	1132.8	1132.6	1132.8	1133.7	1134.6	1135.2
1.9	6.2	9.2	9.4	9.2	8.3	7.4	6.8
7	8.0	7	1.6	2.4	2.7	3.7	7.0
1139.6	1138.9	1132.3	1132.3	1132.9	1134.6	1134.9	
2.4	3.1	9.7	9.7	9.1	7.4	7.1	
0.0	7	12	17	37	42	8.0	

Sta	BS	HI	FS	Elev
Sta 65+00		1139.63		
Sta 66+0.0				
TP	4.58	1139.33	4.88	1134.75

67+00.

67+65

68+00

68+25

69+00

70+00

TP	5.00	1136.21	8.12	1131.21
----	------	---------	------	---------

71+0.0

72+00

72+15

72+90

1134.8 4.8 00	1134.5 5.1 8	1134.8 7.8 13	1131.7 7.9 27	1132.4 7.2 25	1133.1 6.5 29	1133.8 5.8 39	1134.6 5.0 80
1134.9 4.7 00	1134.0 5.2 17	1131.2 8.4 20	1131.1 8.5 28	1131.3 8.3 33	1133.5 6.1 40	1133.5 6.1 80	

1134.0 5.3 00	1133.4 5.9 15	1132.3 7.0 19	1131.1 8.2 33	1132.7 6.6 41	1133.0 6.3 49	1134.0 5.3 80
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------

1132.8 6.5 00	1133.1 6.2 20	1130.3 9.0 25	1130.3 9.0 35	1131.5 7.8 39	1132.6 6.7 45-80	1131.5 7.8 80
---------------------	---------------------	---------------------	---------------------	---------------------	------------------------	---------------------

1134.5 4.8 00	1134.0 5.3 34	1130.8 9.3 38-80
---------------------	---------------------	------------------------

1134.2 5.1 00	1133.3 6.0 80
---------------------	---------------------

1131.9 7.4 00	1131.9 7.4 43	1129.9 10.5 49	1129.3 10.0 60	1131.1 8.2 66	1133.6 5.7 80
---------------------	---------------------	----------------------	----------------------	---------------------	---------------------

1130.6 8.7 00-8	1129.0 10.3 15	1130.0 9.3 29	1129.1 10.2 52	1133.4 5.9 80	1132.8 6.5 80	1131.8 7.5 115
-----------------------	----------------------	---------------------	----------------------	---------------------	---------------------	----------------------

1131.1 5.1 00	1131.8 9.9 12	1128.8 7.4 20	1128.4 7.8 33	1130.4 5.8 37	1131.6 4.6 65-80
---------------------	---------------------	---------------------	---------------------	---------------------	------------------------

1132.7 3.5 00	1130.2 6.0 57	1129.1 9.1 61	1127.9 8.3 74	1128.6 7.6 79	1130.0 6.2 86
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------

1134.5 1.7 00-8	1130.2 6.0 41	1129.3 6.9 68	1127.2 9.6 73	1127.2 9.0 80	1127.9 8.3 86	1128.9 7.3 94	1129.2 7.0 100
-----------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	----------------------

1133.4 2.8 00	1132.1 9.1 50	1133.4 2.8 76	1127.7 8.5 96	1128.1 8.1 128	1129.2 7.0 140
---------------------	---------------------	---------------------	---------------------	----------------------	----------------------

Sta	BS	HI	IS	Elev
TP	4.54	1132.69	7.06	1128.10
79+75				

80+00 Brook enters from left

80+50

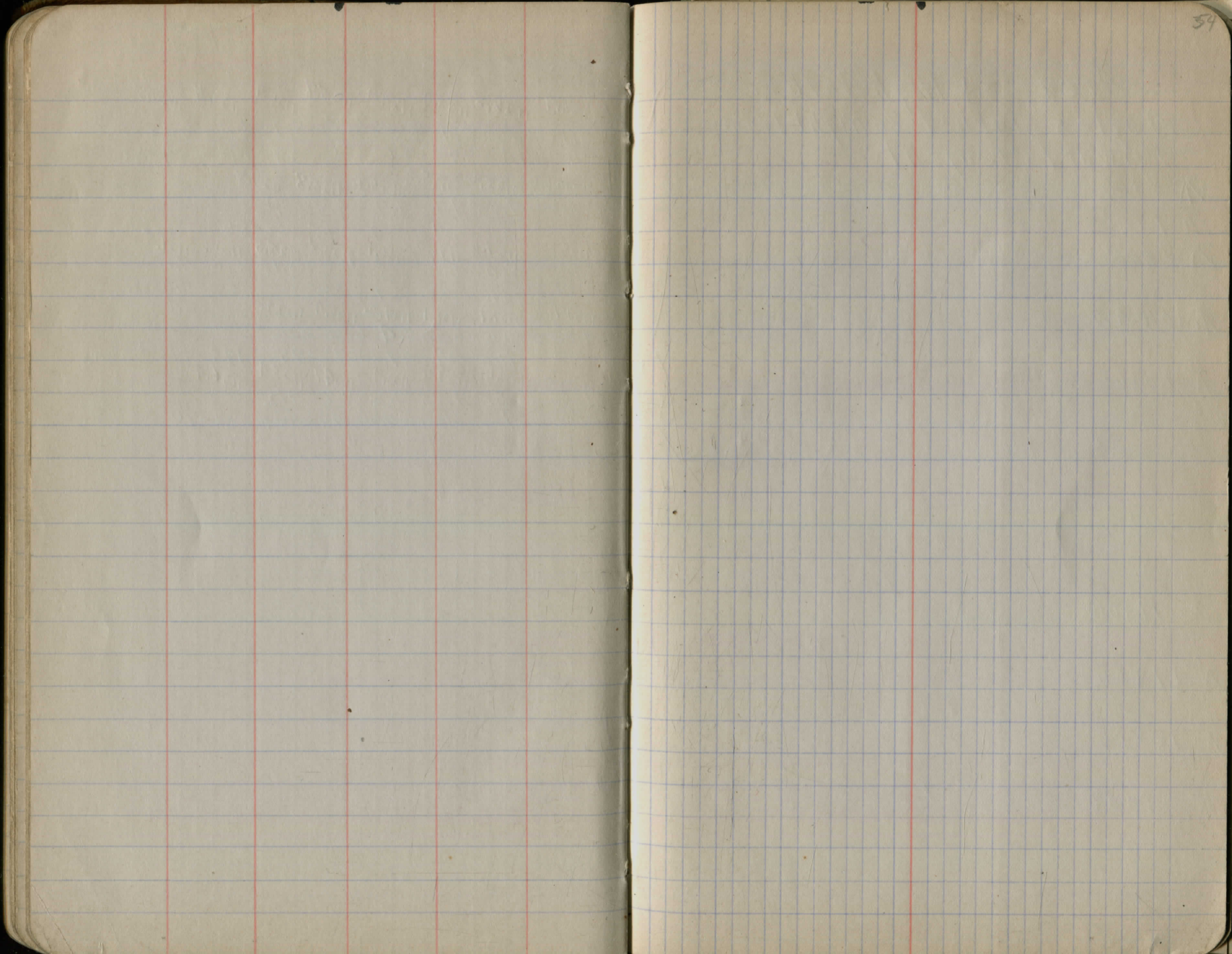
81+00

81+79.5

1126.9	1126.2	1125.9	1124.1	1125.8	1126.9	1126.5	1127.5
5.7	6.4	8.7	8.5	6.8	5.7	6.1	5.1
06	14	17	27	30	37	48	57-80

1126.0	1125.6	1125.0	1124.9	1125.8	1127.5		
6.6	7.0	7.6	7.7	6.8	5.1		
80	21	27	39	75	56-80		
1128.0	1127.6	1126.0	1126.1	1123.8	1129.5	1126.6	1127.5
4.6	5.0	6.6	6.5	8.8	8.1	6.0	5.1
20	19	22	29	36	60	65	70-80

1128.7	1127.9	1126.1	1127.2	1126.4	1127.2		
8.9	9.7	6.5	5.9	6.2	5.9		
00	16	27	47	69	75		
1126.2	1124.1	1123.6	1123.4	1124.7	1125.4	1126.4	175-195 banks
6.9	8.5	9.0	9.2	7.9	7.2	6.2	
00	7	12	42	48	51	56-80	



Area of High Water.
 Angles Turned to Right from
 Forward Tangent

π 8+00

π 9+00

π 10+40

π 13+00

π 16+00

π 17+00

π 18+00

π 19+00

Angle

Distance

90°

100'

90°

12'

90°

15'

90°

175'

270°

20'

90°

125'

38-30

180

86-30

75

126-15

140

187-45

150

324

60

332

140

354

710

90

125

270

8

90

100

270

10

90

125

270

5

90

80

270

25

326

140

320

155

π 19400

continued

Point A turned from ^{Sta} 17-19 extended
as above readings

π Point A

Angle

Distance

298

340

294

440

311

420

339

320

356

230

39

165

66

360

72

255

89

300

70

360

310-55

430

323 N. side

125

357 " "

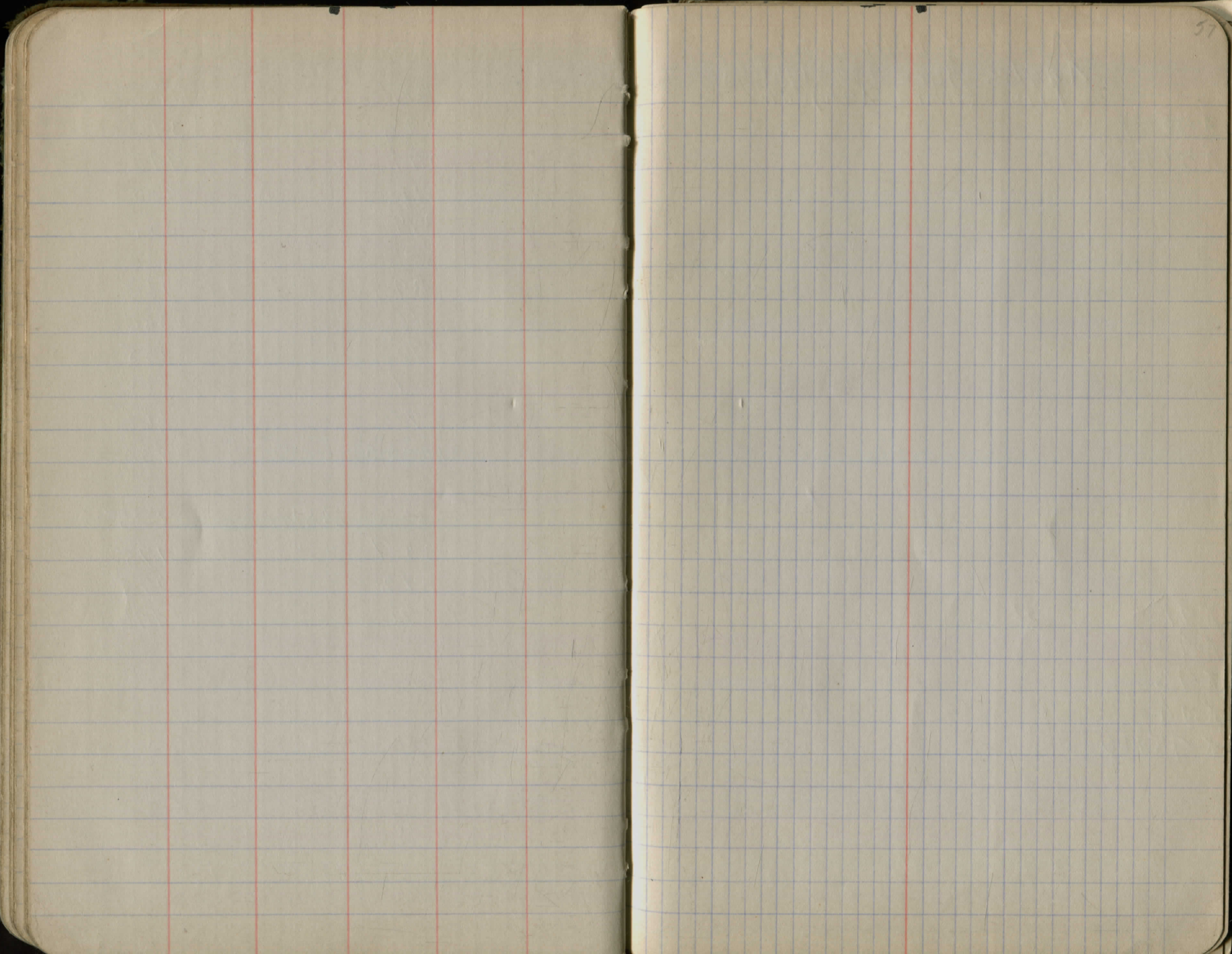
175

12

275

20

440



Area of High Water
 Angles Turned to right
 From forward Tangent

π 35+00
 π 36+50

π 41
 π 42
 π 43
 π 44
 π 45+00

58

Angle	Distance
90	N. bank of outlet
131	380
131 S. side	60
110	225
83	260
61	300
61 S. side	55
40	330
23	370
17	440
17 S. side	100
03 S. side	216
356 "	290
357 "	360
01 "	400
90 S. side	15
90 S. side	15
90 " "	05
90 " "	00
158	390
158 S. side	25
148	230
103	100
77	150
35	200
00 S. side	100

45+00

Continued

49+57.4

51+08.5

58+60.5

Angle

Distance

343 S.S. side 165

340 S.S. side 330

265 35

90 75

209-30 145

196-30 135

97 70

20 180

23 280

15 320

07 390

05 570

223 130

190 25

328 160

352 340

358 540

154 420

143 460

132 410

102 260

75 220

75 280

49 210

58+60.5 continued

64+50

Middle of culvert S. Side

Middle of creek + Outlet

Spring enters

Creek enters

Angle

236

239

209

189

132

124

114

113

99

100

95

96

100

163

126

21

172

176

175

181

215

189

04

04-30

00

65
Distance

180

140

100

40

255

400

460

600

580

930

480

375

320

100

65

200

250

260

220

150

120

120

30

250

340

68+18.3

Creek

72+00

Middle of culvert

Angle

218

218

246

246

308

06

306

335

01

73

89

83-30

76

71

52

55

50

45

28

08

23

35

25

6

15

Distance

320

340

220

235

75

130

140

140

195

130

220

240

210

150

210

225

240

225

170

210

110

105

65

90

115

75+00

78+00

60
Angle

Distance

146

75

147

95

116

70

18

80

28

95

26

156

22

215

19

245

40

40

4

8

350

90

356

146

5

200

156

45

270

65

320

75

333

145

333

180

351

200

115

130

73

165

59

150

42

200

41

260

47

280

81+00

in creek

Angle

63
Distance

194

70

228

70

195

60

117

30

18

15

355

90

103

255

85

215

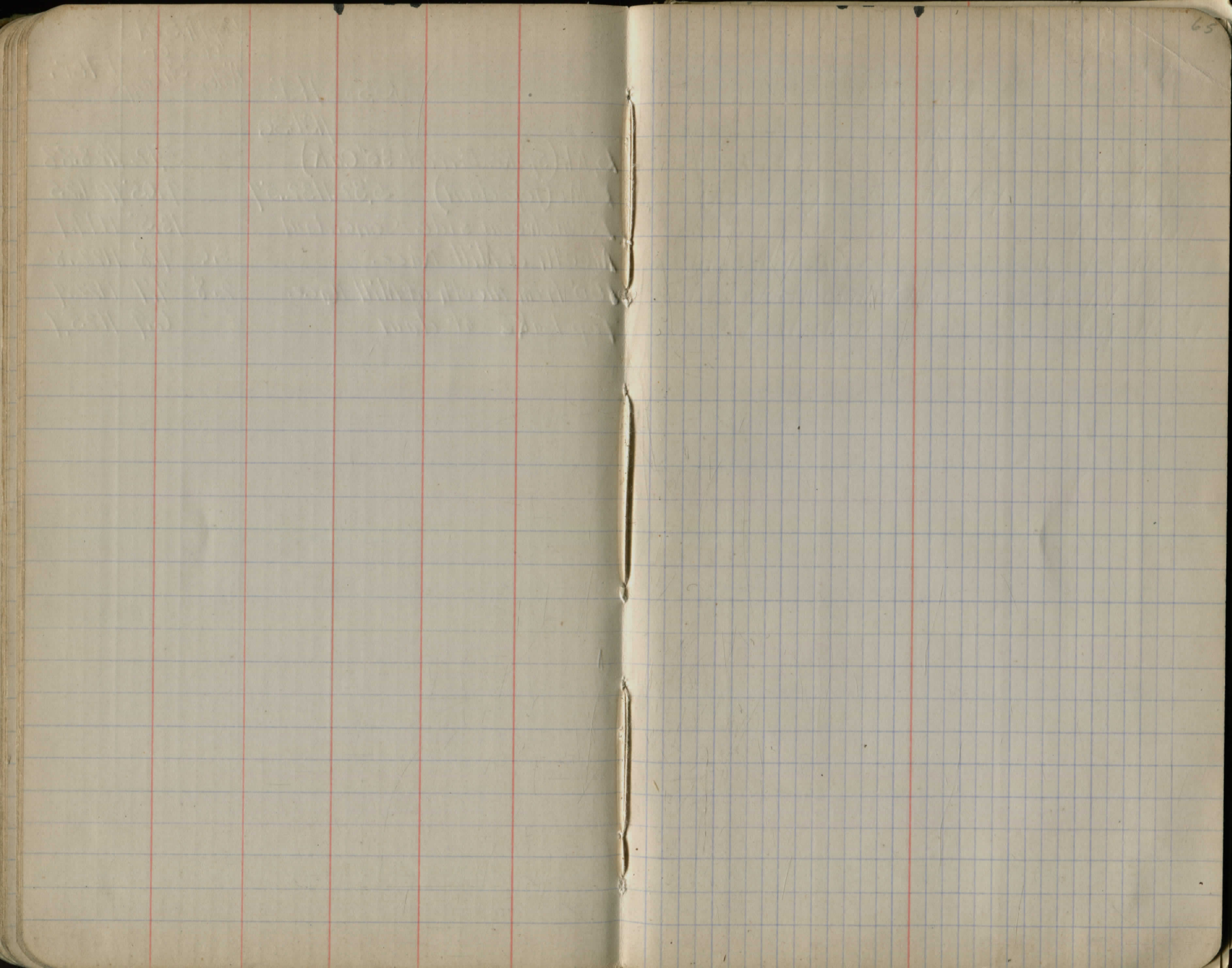
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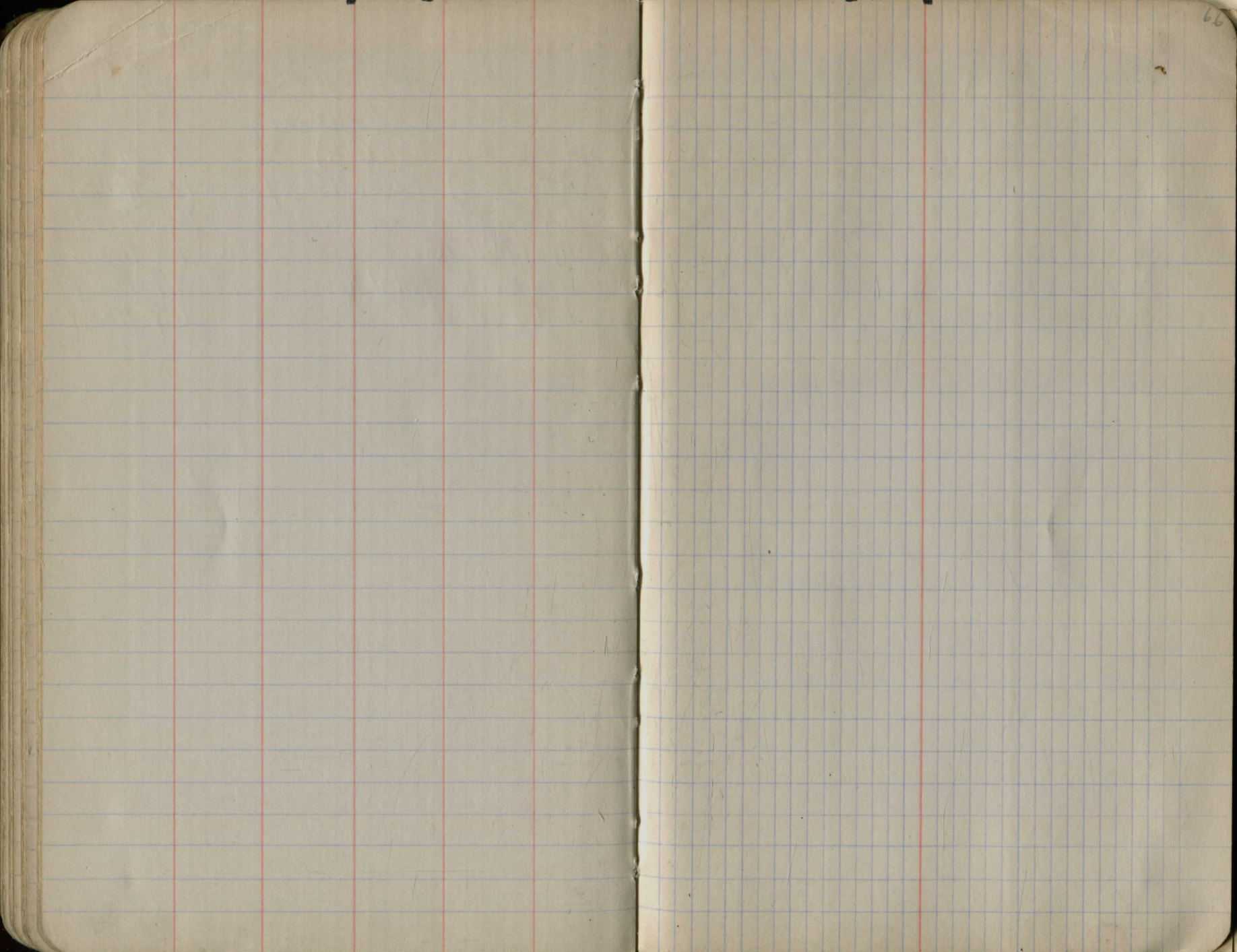
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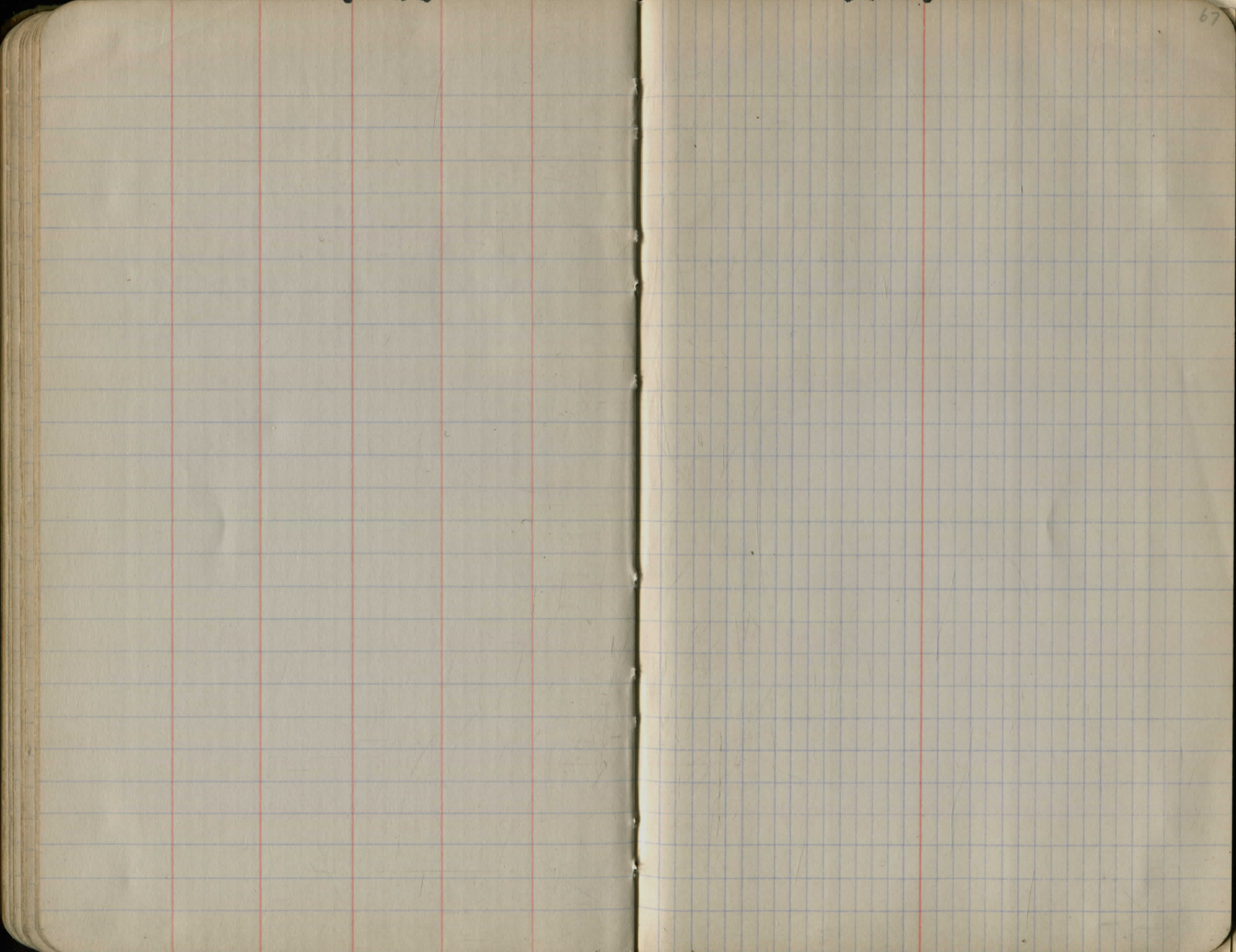
Cont. from pg 16 (over) in
Back this book.

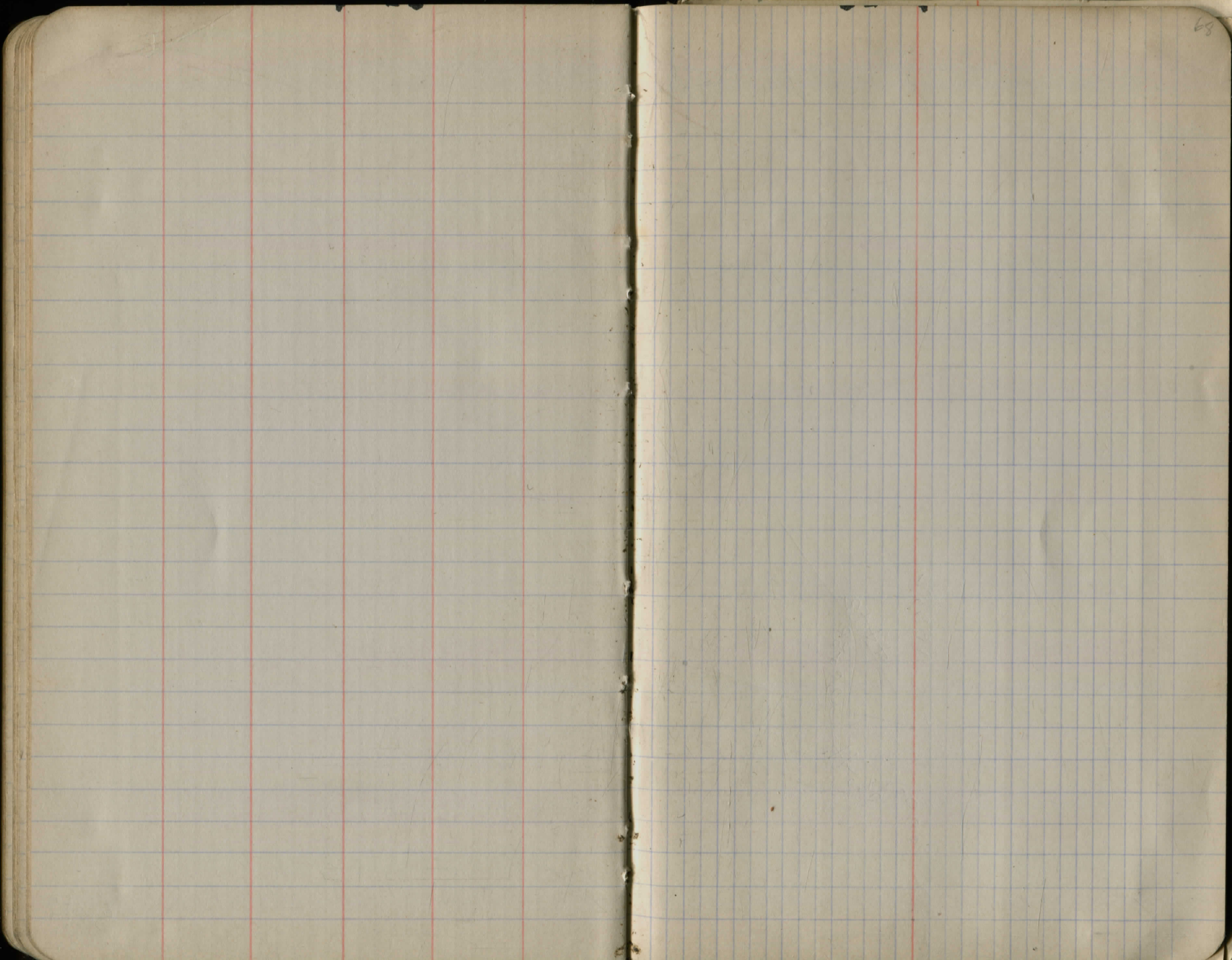
	B.S.	H.I.	Depth of Water	Bed of Stream	Elev.
60+00			0.7	7.1	1132.8
61			0.5	7.6	32.3
62			0.6	8.2	31.7
63			0.8	8.7	31.2
64			1.0	9.4	30.5
TP ^{Noon}	3.71	1137.72		5.90	1134.01
65+00			1.7	9.4	28.3
66			1.7	9.6	28.1
67			0.5	9.0	28.7
68			1.1	10.2	27.5
69			3.0	12.5	25.2
70			3.8	14.1	23.6
B.M.	3.35	1134.41		6.65	^{1131.06} 1131.07
↖ Nail N. root 30" maple Sta 71+26 Lt 22'					
71+00			0.7	8.4	1126.0
72+00			1.0	9.3	1125.1
73+00			1.4	9.9	1124.5
74			0.5	9.1	25.3
75+00			1.1	9.7	24.7
T.P.	5.09	1139.03		0.47	1133.94
78+00			2.9	16.3	1122.7
TP	5.50	1140.76		3.77	1135.26
82+00 (stream = 30' wide)			1.6	16.6	24.2
83+00			2.3	17.4	23.4
T.P.	0.46	1134.30		6.92	1133.84

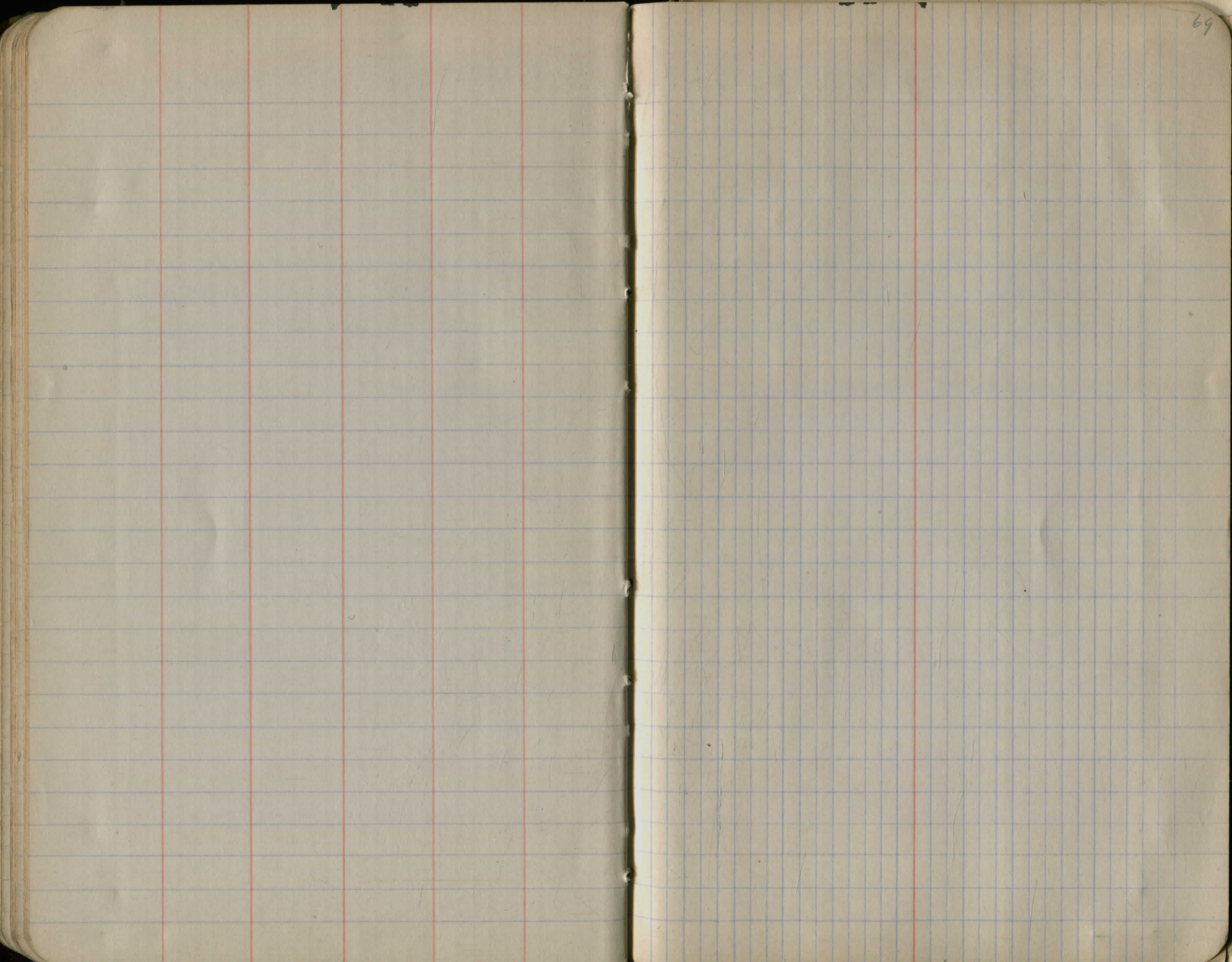
	B.S.	H.I.	Depth of Water	Bed of Stream	Elev.
		1134.30			
B.M. (Spike E. root 30" Oak)				5.42	1128.88
B.M. (Top dam)	5.32	1132.57		7.05	1127.25
Downstream side Conc. dam				13.5	1119.1
Mouth of Mill Race			3.0	9.8	1122.8
100' from mouth of Mill Race			2.8	9.7	1122.9
Top Lake at dam				6.9	1125.7

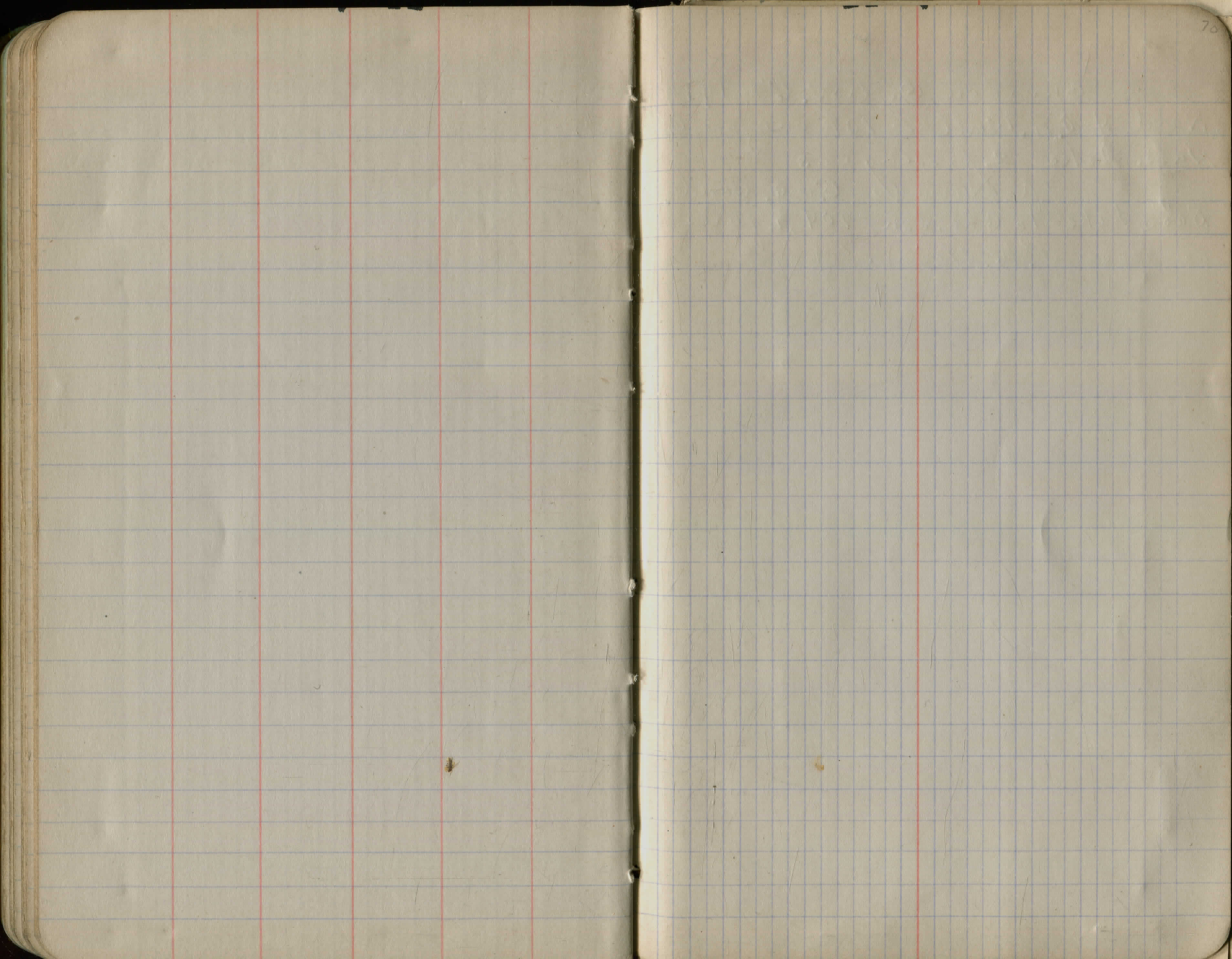












Chardon O. Nov. 6th - 1919

Recd of E. A. Tiedler 10¢ car fare

to Bass Lake 2 passengers

P. R. Haines C. & E. Cond.

Bass Lake to Chardon 10¢, 2 fares

as above P. R. Haines

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1% to 1.
If ground is nearly level, the cut or fill stake
is located by the double entry method in

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of
any other degree, divide by degree of curve
and connection found in column of constants.
Degree of curve with a given L may be found
by dividing tangent (or external), opposite L
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

INDEX

Line and Topo.

Pages 2-12

Levels

" 15-19

Bass Lake Outlet Ditch
Munson Twp.
Geauga Co
1934

12-3-34
rudy - Cold

Davidson
Sperry
Rassback
Hill.

9+00

8+00

7+00

6+00

5+00

(30^{±5})

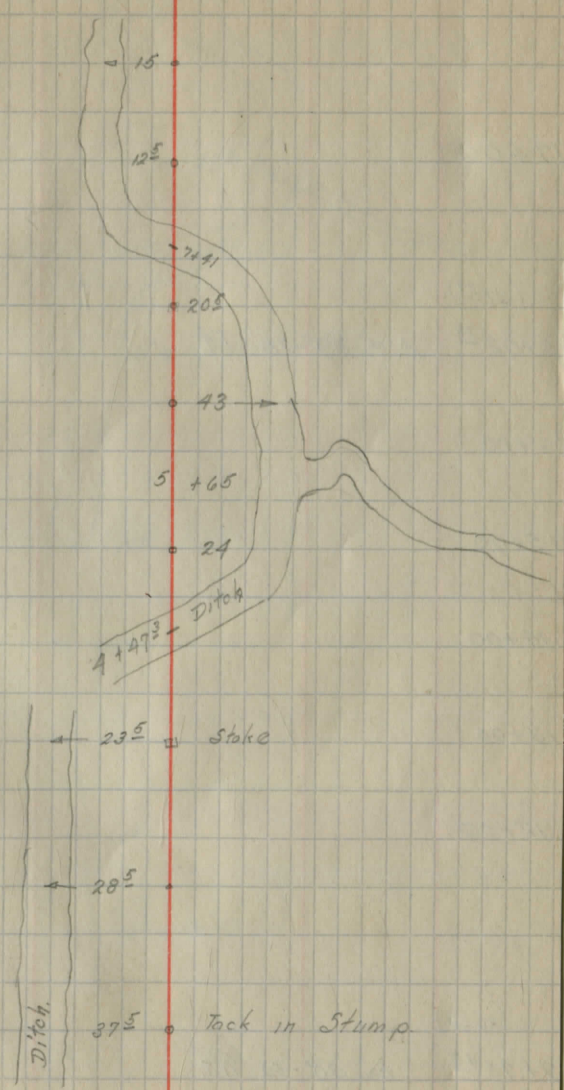
4+19^{±5}

Δ 45°-08' Lt.

2+00

1+00

582
19
47



17+00

(97²⁷)

16+02²³ $\Delta = 39^{\circ}-28' \text{ Lt.}$

16+00

15+00

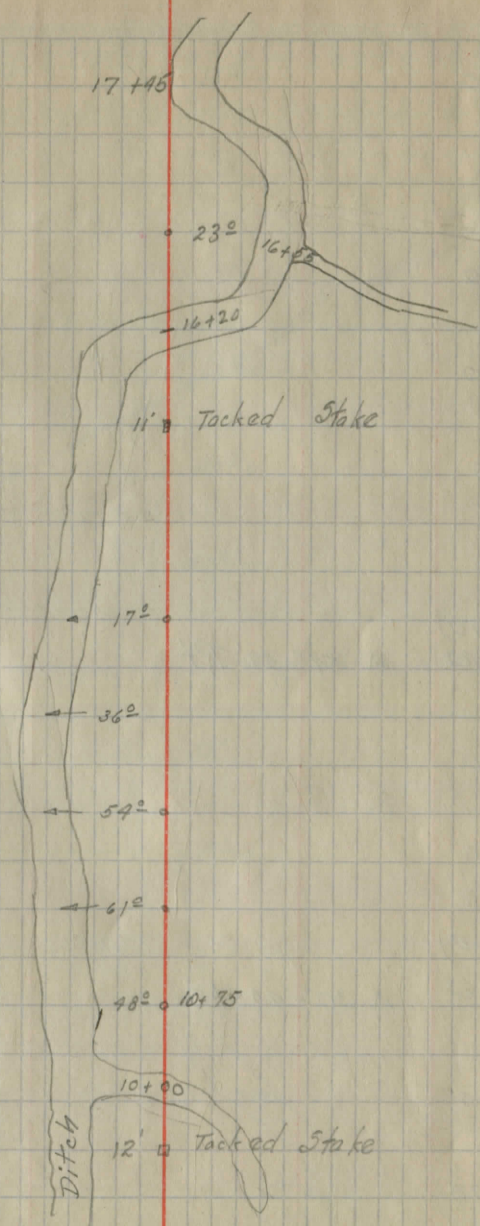
14+00

13+00

12+00

(26³⁵)

9+73⁴⁵ $\Delta = 30^{\circ}-55' \text{ Rt.}$



27+00

26+00

25+00

24+00

23+00

22+00

(4923)
21+50²³

Δ 54°-54' RT

21+00

20+00

(85²³)

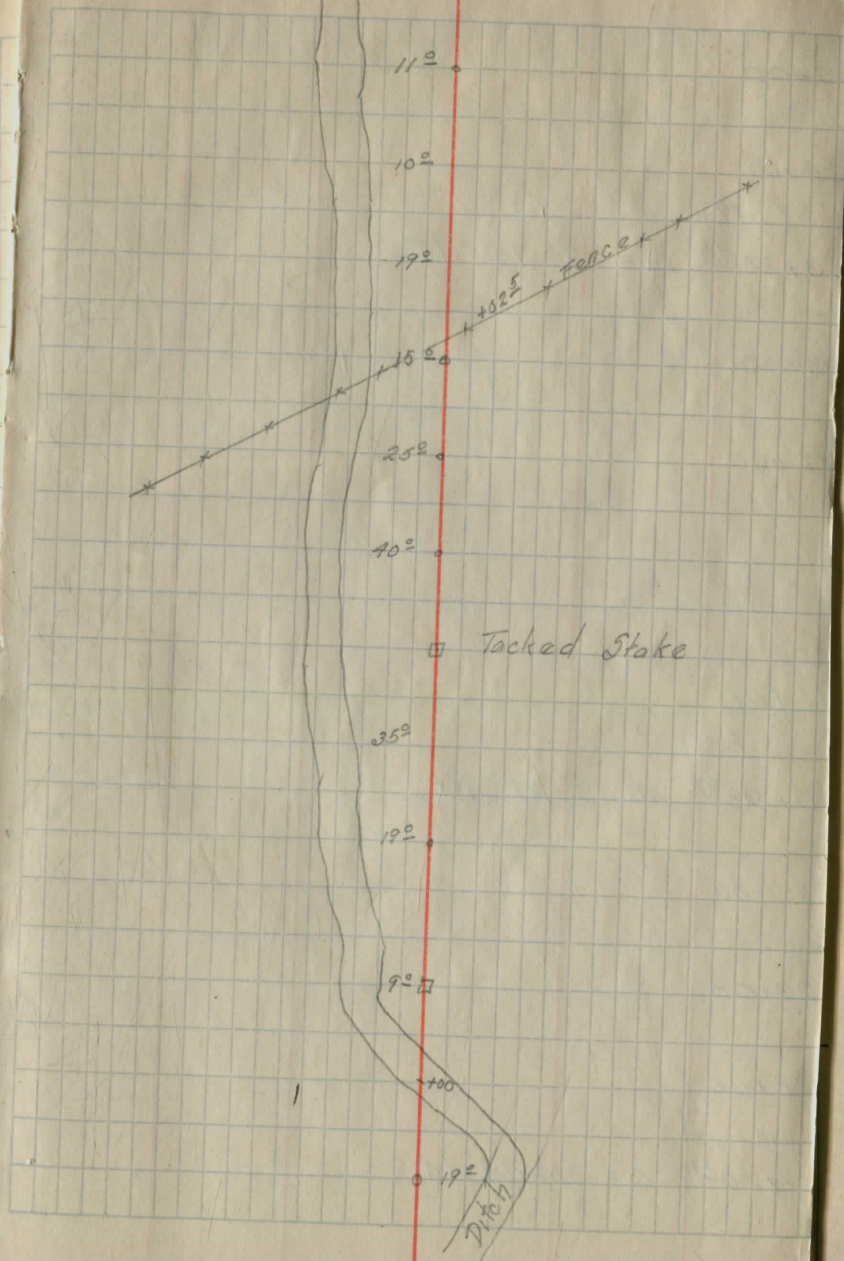
19+14⁶³

Δ 30°-45' LT

19+00

18+00

4



35+00

34+00

(11.57)

33+88²³ $\Delta = 7^\circ - 14'$ Lt.

33+00

32+00

31+00

(6.07)

30+93²³ $\Delta = 19^\circ - 22'$ Rt.

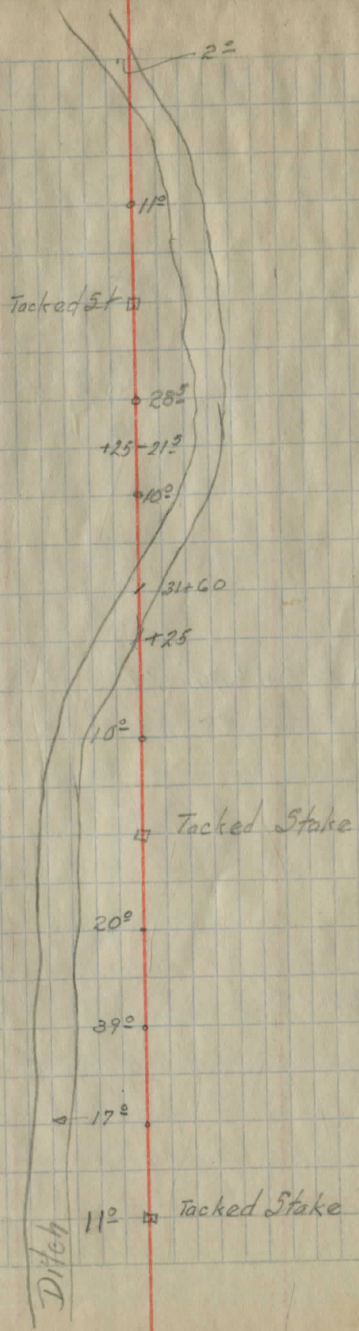
30+00

29+00

28+00

No. 07 (7.97)

27+00²³ $\Delta = 10^\circ - 44'$ Lt.



45+00

44+00

43+00

42+00

41+00

(78²⁷)

40+21.03 $\Delta = 4^{\circ} 46' 15''$

40+00

39+00

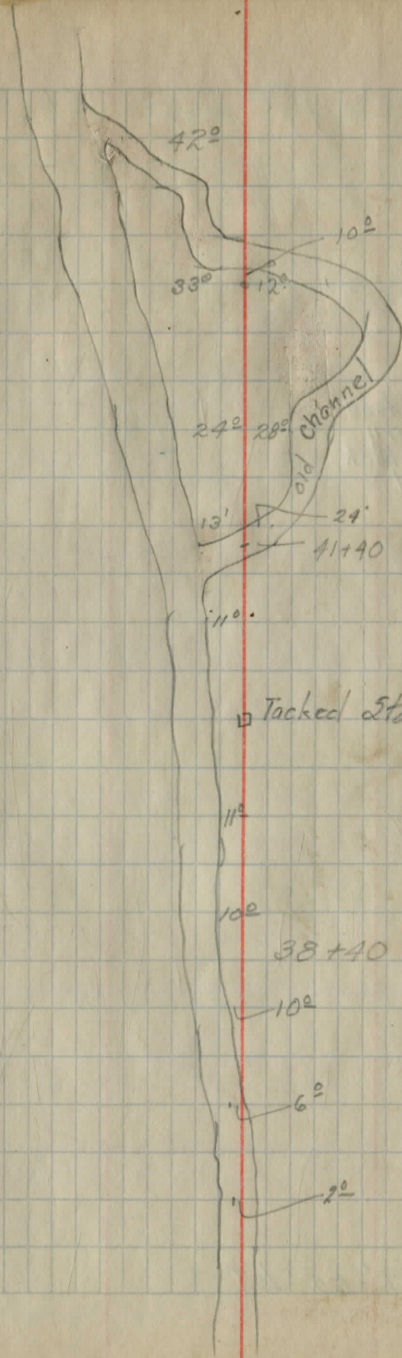
38+00

37+00

36+00

555 = 14
(Nearle)

6



19+00

18+00

17+00

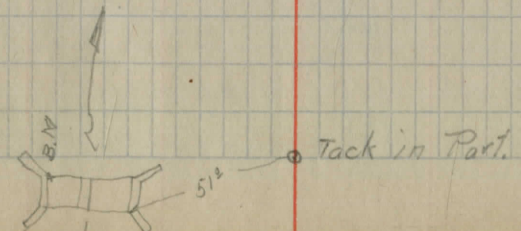
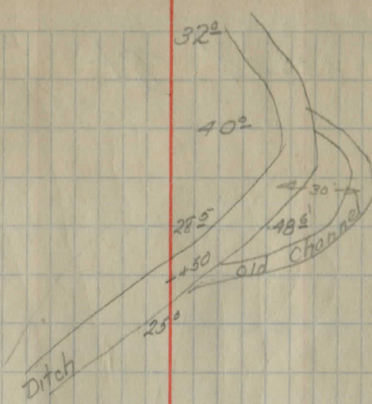
16+00

3/2-4-34
Windy - Windy
Cold

Davidson
Sperry
Roosback
Hill

(72⁰⁰)

15+27²⁴ Δ 7°-05' Lt.



(22⁴¹)

58+77⁵⁹ Δ 54°-44' Rt.

58+00

57+00

56+00

55+00

(62²⁰)

54+37¹⁹ Δ = 41°-30' Lt.

54+00

53+00

End New Channel

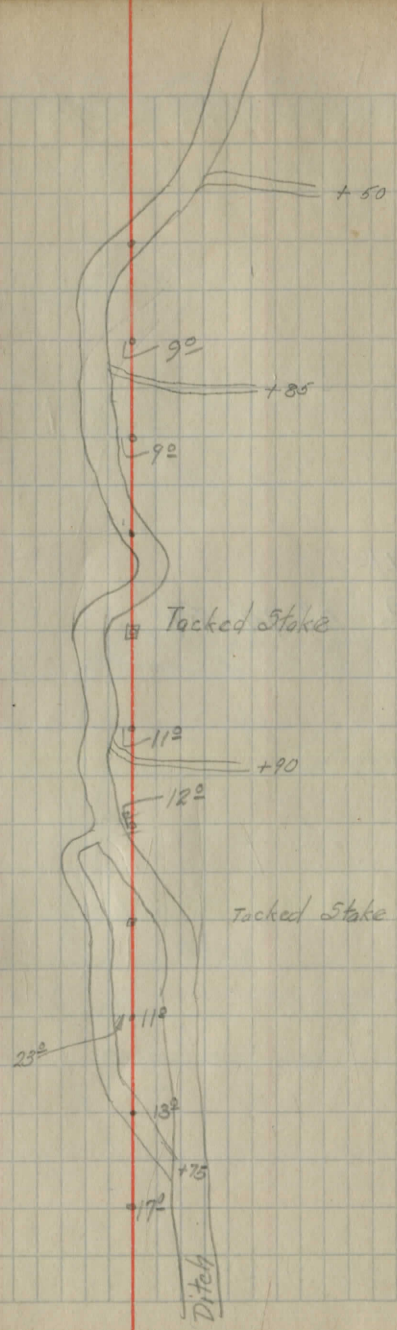
(60⁵²)

52+39¹³ Δ 39°-17' Rt.

52+00

51+00

50+00



267+00

266+00

265+00

(10^{ft})

264+89⁹⁹ 0°-44' Rt.

264+00

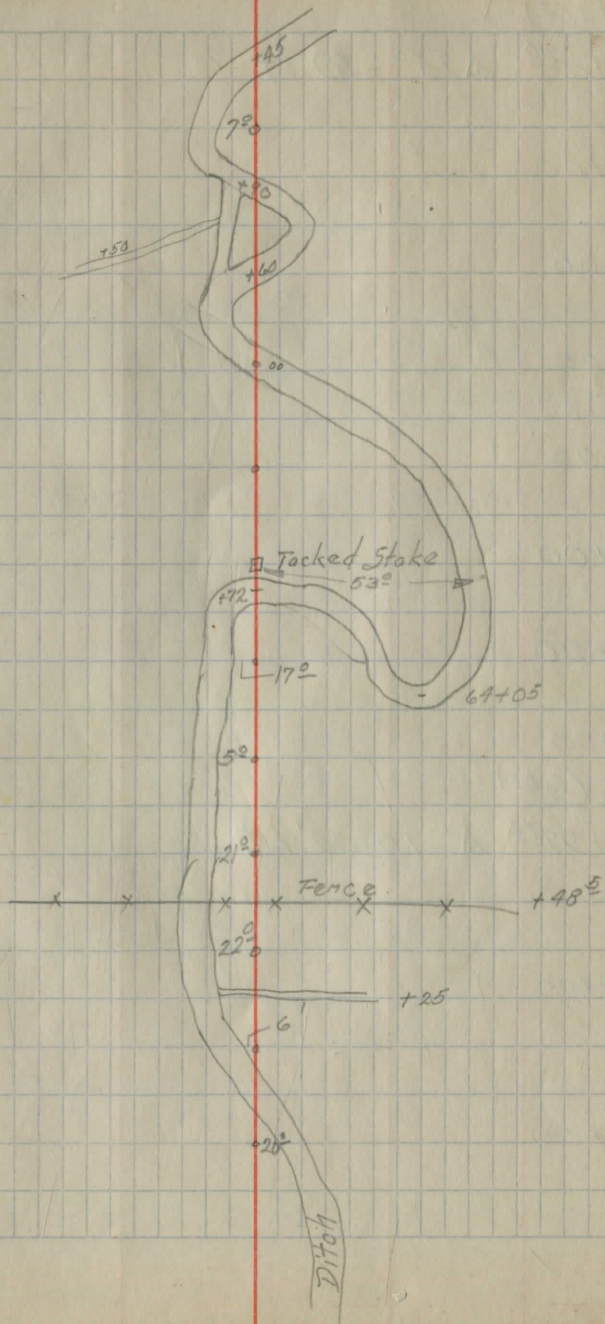
263+00

262+00

261+00

260+00

259+00



(51¹⁰)

62 6+48⁹⁰ $\Delta 25^\circ - 59$ Lt

76+00

5 5+00

32 4+00

32 3+00

67 2+00

11 71+00

20 2+00

30 (2²⁰)

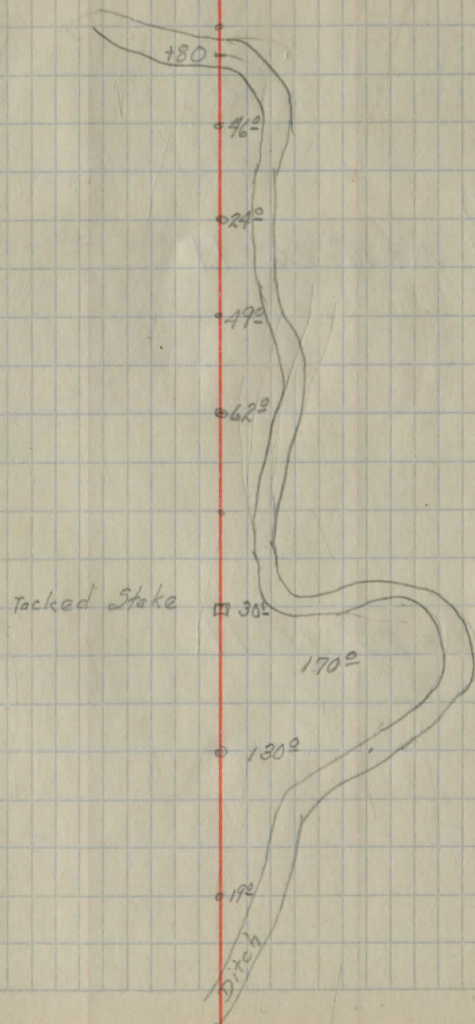
19 9+97²² $\Delta 10^\circ 34'$ Lt

69+00

68+00

10

10



92+00²⁹

Stadia Reading $6 \frac{35}{100}$ to Dam
Vert Angle $0^{\circ} 30' = 635^{\circ}$

85+65²⁵ $\Delta = 52^{\circ} - 01' Lt.$

85+00

84+00

83+00

(62²²)

82+37²¹ $\Delta = 16^{\circ} - 26' Lt.$

82+00

81+00

80+00

(99¹²)

79+00²⁰ $\Delta = 29^{\circ} - 15' Lt.$

78+00

77+00

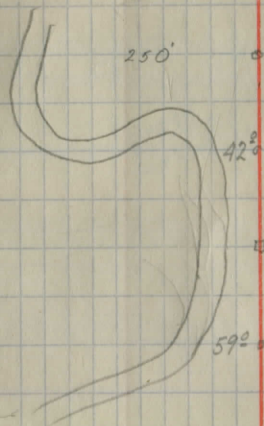
S 120 W
(Needle)

□ B.M. on Dam.

11

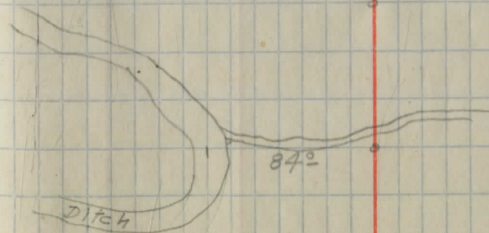
11

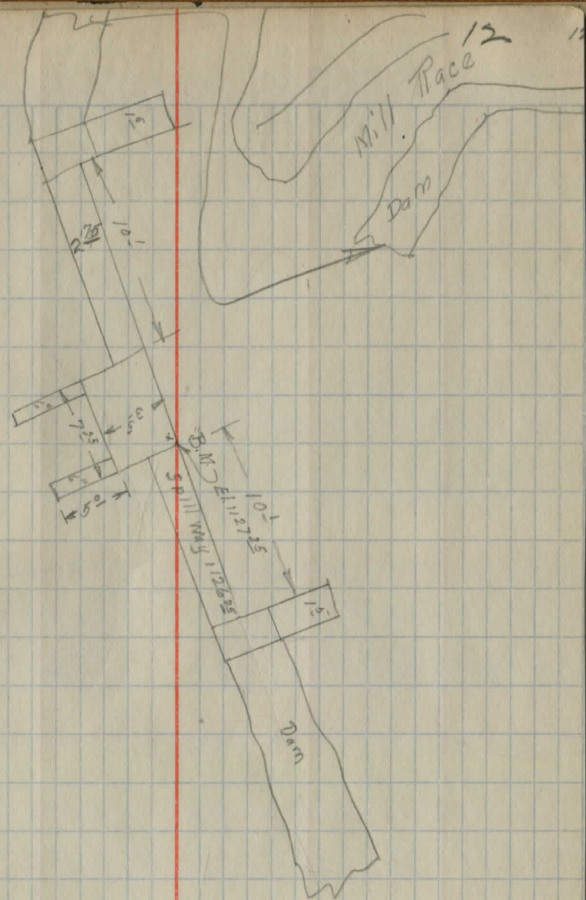
□ Tacked Stake



□ Tacked Stake

□ Tacked Stake





14

12-5-34
cloudy-coldDavidson
Sperry
Rossback
Hill
(+)

(H.I.)

LEVELS(Depth of H₂O)(-)
(Bed of Stream)

(Elev)

B.M.	5.36	1149.42			1144.06
0+00			1.0	8.8	1140.6
1+00			2.0	9.9	1139.5
2+00			1.5	9.5	1139.9
3+00			0.8	8.8	1140.6
4+00			1.2	9.6	1139.8
5+00			1.0	9.6	1139.8
T.P.	4.21	1148.08		5.55	1143.87
6+00			1.0	8.3	1139.8
7+00			1.4	8.7	1139.4
8+00			1.9	9.9	1138.2
9+00			1.8	9.1	1139.0
10+00			2.0	9.4	1138.7
T.P.	5.95	1148.20		5.13	1142.95
11+00			1.6	9.9	1139.0
12+00			1.7	10.0	1138.9
13+00			1.4	9.7	1139.2
14+00			1.8	10.1	1138.8
15+00			1.8	10.2	1138.7
16+00			2.4	10.8	1138.1
B.M.				6.92	1141.98
17+00			1.5	10.2	1138.7
T.P.	3.48	1146.36		6.02	1142.88

15

Spike in NW Root of Elm at Outlet of Bass Lake
Sta 0+56 Lt 60'

Stream 15' Wide

Stream 15' Wide

Nail & Wash on S. Root 30" Maple Sta 15+25 Rt. 55'

1144.58

Depth
of
Water

Bed
of
stream

37+00		1.0	8.1	1136.5
38+00	Stream=11' wide	1.1	8.6	1136.0
39+00		0.5	8.8	1135.8
40+00		0.9	9.4	1135.2
41+00	Strm=16'	2.0	11.1	1133.5
T.P.	5.15 1143.04		6.69	1137.89
42+00	(old channel 1135.3)	1.0	8.7	1134.3
43+00	" " = 35.0	2.3	10.0	1133.0
44+00	" " = 34.7	2.4	10.1	1132.9
45+00		1.6	9.3	1133.7
B.M.	8.57 1142.14		6.6	1141.57
46+00	X in N. wall of bridge at angle with Wing wall Sta 46+00	1.9	9.1	1133.0
47+00		0.8	8.2	1133.9
48+00		1.6	8.9	1133.2
49+00		2.2	9.5	1132.6
50+00		1.8	9.1	1133.0
51+00		0.7	8.1	1134.0
52+00		2.3	9.7	1132.4
53+00		0.7	8.1	1134.0
T.P.	4.50 1140.67		5.97	1136.17
54+00		0.6	6.9	33.8
55+00		1.5	8.0	32.7
56		1.0	7.5	33.2
57		0.9	7.5	33.2
58+00		1.1	7.8	32.9
T.P.	4.44 1139.91		5.20	1135.47
59+00	(cont. pg. 64)	1.3	7.4	1132.5

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388	T	20'	568.53	28.137	T	20'	1079.2	100.75	T
30'	75.01	.491	.03	30'	576.95	28.974	.03	30'	1087.8	102.35	.03
40'	83.34	.606	E	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	.001	50'	593.79	30.686	.06	50'	1105.1	105.60	.13
2°	100.01	.873	10° C.	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024	T	10'	610.64	32.447	T	10'	1122.4	108.90	T
20'	116.68	1.188	.06	20'	619.07	33.347	.06	20'	1131.0	110.57	.06
30'	125.02	1.364	E	30'	627.50	34.259	E	30'	1139.7	112.25	E
40'	133.36	1.552	.003	40'	635.93	35.183	.011	40'	1148.4	113.95	.013
50'	141.70	1.752	T	50'	644.37	36.120	T	50'	1157.0	115.66	T
3°	150.04	1.964	15° C.	13°	652.81	37.070	.011	23°	1165.7	117.38	.013
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.13
30'	175.06	2.674	E	30'	678.15	39.993	E	30'	1191.8	122.63	.19
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	.013
50'	191.74	3.207	T	50'	695.06	42.004	T	50'	1209.2	126.20	.025
4°	200.08	3.492	15° C.	14°	703.51	43.029	.011	24°	1217.9	128.00	.013
10'	208.43	3.790	T	10'	711.97	44.066	T	10'	1226.6	129.82	T
20'	216.77	4.099	.06	20'	720.44	45.116	.06	20'	1235.3	131.65	.06
30'	225.12	4.421	E	30'	728.90	46.178	E	30'	1244.0	133.50	E
40'	233.47	4.755	.003	40'	737.37	47.253	.011	40'	1252.8	135.35	.013
50'	241.81	5.100	T	50'	745.85	48.341	T	50'	1261.5	137.23	T
5°	250.16	5.459	15° C.	15°	754.32	49.441	.011	25°	1270.2	139.11	.013
10'	258.51	5.829	T	10'	762.80	50.554	.19	10'	1279.0	141.01	.29
20'	266.86	6.211	.06	20'	771.29	51.679	.13	20'	1287.7	142.93	.13
30'	275.21	6.606	E	30'	779.77	52.818	E	30'	1296.5	144.85	.19
40'	283.57	7.013	.004	40'	788.26	53.969	.017	40'	1305.3	146.79	.038
50'	291.92	7.432	T	50'	796.75	55.132	T	50'	1314.0	148.75	.046
6°	300.28	7.863	15° C.	16°	805.25	56.309	.011	26°	1322.8	150.71	.013
10'	308.64	8.307	T	10'	813.75	57.498	.19	10'	1331.6	152.69	.13
20'	316.99	8.762	.06	20'	822.25	58.699	.13	20'	1340.4	154.69	.13
30'	325.35	9.230	E	30'	830.76	59.914	E	30'	1349.2	156.70	.19
40'	333.71	9.710	.003	40'	839.27	61.141	.011	40'	1358.0	158.72	.013
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	.025
7°	350.44	10.707	15° C.	17°	856.30	63.634	.011	27°	1375.6	162.81	.013
10'	358.81	11.224	T	10'	864.82	64.900	.19	10'	1384.4	164.86	.13
20'	367.17	11.753	.06	20'	873.35	66.178	.13	20'	1393.2	166.95	.13
30'	375.54	12.294	E	30'	881.88	67.470	E	30'	1402.0	169.04	.19
40'	383.91	12.847	.003	40'	890.41	68.774	.011	40'	1410.9	171.15	.013
50'	392.28	13.413	T	50'	898.95	70.091	T	50'	1419.7	173.27	.025
8°	400.66	13.991	15° C.	18°	907.49	71.421	.011	28°	1428.6	175.41	.013
10'	409.03	14.582	T	10'	916.03	72.764	.19	10'	1437.4	177.55	.13
20'	417.41	15.184	.06	20'	924.58	74.119	.13	20'	1446.3	179.72	.13
30'	425.79	15.799	E	30'	933.13	75.488	E	30'	1455.1	181.89	.19
40'	434.17	16.426	.003	40'	941.69	76.869	.011	40'	1464.0	184.08	.013
50'	442.55	17.065	T	50'	950.25	78.264	T	50'	1472.9	186.29	.025
9°	450.93	17.717	15° C.	19°	958.81	79.671	.011	29°	1481.8	188.51	.013
10'	459.32	18.381	T	10'	967.38	81.092	.19	10'	1490.7	190.74	.13
20'	467.71	19.058	.06	20'	975.96	82.525	.13	20'	1499.6	192.99	.13
30'	476.10	19.746	E	30'	984.53	83.972	E	30'	1508.5	195.25	.19
40'	484.49	20.447	.003	40'	993.12	85.431	.011	40'	1517.4	197.53	.013
50'	492.88	21.161	T	50'	1001.7	86.904	T	50'	1526.3	199.82	.025
10°	501.28	21.887	15° C.	20°	1010.3	88.389	.011	30°	1535.3	202.12	.013
10'	509.68	22.624	T	10'	1018.9	89.888	.19	10'	1544.2	204.44	.13
20'	518.08	23.375	.06	20'	1027.5	91.399	.13	20'	1553.1	206.77	.13
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	.19
40'	534.89	24.913	.003	40'	1044.7	94.462	.011	40'	1571.0	211.48	.013
50'	543.29	25.700	T	50'	1053.3	96.013	.034	50'	1580.0	213.86	.025

T = R tan ½ I

E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	887.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	890.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	894.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	.03	30'	2170.8	897.4	.03	30'	2763.7	631.7	.03
40'	1624.9	226.0	.13	40'	2180.3	900.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	904.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	907.6	.037	52°	2794.5	645.2	.056
10'	1652.0	233.4	T	10'	2209.0	911.1	T	10'	2804.9	649.7	T
20'	1661.0	235.9	.06	20'	2218.6	914.5	.06	20'	2815.2	654.3	.06
30'	1670.0	238.4	E	30'	2228.1	918.0	E	30'	2825.6	658.8	E
40'	1679.1	241.0	.013	40'	2237.7	921.4	.017	40'	2835.9	663.4	.017
50'	1688.1	243.5	T	50'	2247.3	925.0	T	50'	2846.3	668.0	T
33°	1697.2	246.1	10° C.	43°	2257.0	928.5	.075	53°	2856.7	672.7	.112
10'	1706.3	248.7	T	10'	2266.6	932.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.26	20'	2276.2	935.6	.34	20'	2877.5	682.0	.34
30'	1724.4	253.9	E	30'	2285.9	939.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	.046	40'	2295.6	942.8	.075	40'	2898.4	691.4	.075
50'	1742.6	259.1	T	50'	2305.2	946.4	T	50'	2908.9	696.1	T
34°	1751.7	261.8	15° C.	44°	2314.9	950.0	.116	54°	2919.4	700.9	.112
10'	1760.8	264.5	T	10'	2324.6	953.6	T	10'	2929.9	705.7	T
20'	1770.0	267.2	.19	20'	2334.3	957.3	.19	20'	2940.4	710.5	.19
30'	1779.1	269.9	E	30'	2344.1	961.0	E	30'	2951.0	715.3	E
40'	1788.2	272.6	.038	40'	2353.8	964.6	.038	40'	2961.5	720.1	.038
50'	1797.4	275.3	T	50'	2363.5	968.4	T	50'	2972.1	725.0	T
35°	1806.6	278.1	15° C.	45°	2373.3	972.1	.075	55°	2982.7	729.9	.075
10'	1815.7	280.8	T	10'	2383.1	975.8	.075	10'	2993.3	734.8	.075
20'	1824.9	283.6	.06	20'	2392.8	979.6	.06	20'	3003.9	739.7	.06
30'	1834.1	286.4	E	30'	2402.6	983.4	E	30'	3014.5	744.6	E
40'	1843.3	289.2	.013	40'	2412.4	987.2	.013	40'	3025.2	749.6	.013
50'	1852.5	292.0	T	50'	2422.3	991.0	T	50'	3035.8	754.6	T
36°	1861.7	294.9	15° C.	46°	2432.1	994.8	.116	56°	3046.5	759.6	.112
10'	1870.9	297.7	T	10'	2441.9	998.7	.116	10'	3057.2	764.6	.112
20'	1880.1	300.6	.19	20'	2451.8	1002.5	.19	20'	3067.9	769.7	.19
30'	1889.4	303.5	E	30'	2461.7	1006.4	E	30'	3078.7	774.7	E
40'	1898.6	306.4	.038	40'	2471.5	1010.3	.038	40'	3089.4	779.8	.038
50'	1907.9	309.3	T	50'	2481.4	1014.3	T	50'	3100.2	784.9	T
37°	1917.1	312.2	15° C.	47°	2491.3	1018.2	.075	57°	3110.9	790.1	.075
10'	1926.4	315.2	T	10'	2501.2	1022.2	.075	10'	3121.7	795.2	.075
20'	1935.7	318.1	.06	20'	2511.2	1026.1	.06	20'	3132.6	800.4	.06
30'	1945.0	321.1	E	30'	2521.1	1030.1	E	30'	3143.4	805.6	E
40'	1954.3	324.1	.013	40'	2531.1	1034.2	.013	40'	3154.2	810.9	.013
50'	1963.6	327.1	T	50'	2541.0	1038.2	T	50'	3165.1	816.1	T
38°	1972.9	330.2	15° C.	48°	2551.0	1042.2	.116	58°	3176.0	821.4	.112
10'	1982.2	333.2	T	10'	2561.0	1046.3	.116	10'	3186.9	826.7	.112
20'	1991.5	336.3	.19	20'	2571.0	1050.4	.19	20'	3197.8	832.0	

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+
10'	3386.3	925.9	5° C.	10'	4099.5	1315.6	5° C.	10'	4908.0	1814.7	5° C.
20'	3397.5	931.6	T	20'	4112.1	1322.9	T	20'	4922.5	1824.1	T
30'	3408.8	937.3	.25	30'	4124.8	1330.3	.30	30'	4937.0	1833.6	.36
40'	3420.1	943.1	E	40'	4137.4	1337.7	E	40'	4951.5	1843.1	E
50'	3431.4	948.9	.080	50'	4150.1	1345.1	.110	50'	4966.1	1852.6	.149
62°	3442.7	954.8	T	72°	4162.8	1352.6	T	82°	4980.7	1862.2	T
10'	3454.1	960.6	5° C.	10'	4175.6	1360.1	5° C.	10'	4995.4	1871.8	5° C.
20'	3465.4	966.5	T	20'	4188.5	1367.6	T	20'	5010.0	1881.5	T
30'	3476.8	972.4	.25	30'	4201.2	1375.2	.30	30'	5024.8	1891.2	.36
40'	3488.3	978.3	E	40'	4214.0	1382.8	E	40'	5039.5	1900.9	E
50'	3499.7	984.3	.100	50'	4226.8	1390.4	.110	50'	5054.3	1910.7	.149
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10'	3522.6	996.2	T	10'	4252.6	1405.7	T	10'	5084.0	1930.4	T
20'	3534.1	1002.3	.51	20'	4265.6	1413.5	.61	20'	5099.0	1940.3	.72
30'	3545.6	1008.3	E	30'	4278.5	1421.2	E	30'	5113.9	1950.3	.86
40'	3557.2	1014.4	.159	40'	4291.5	1429.0	.220	40'	5128.9	1960.2	.220
50'	3568.7	1020.5	T	50'	4304.6	1436.8	T	50'	5143.9	1970.3	.299
64°	3580.3	1026.6	15° C.	74°	4317.6	1444.6	15° C.	84°	5159.0	1980.4	15° C.
10'	3591.9	1032.8	T	10'	4330.7	1452.5	T	10'	5174.1	1990.5	T
20'	3603.5	1039.0	.76	20'	4343.8	1460.4	.91	20'	5189.3	2000.6	.91
30'	3615.1	1045.2	E	30'	4356.9	1468.4	E	30'	5204.4	2010.8	E
40'	3626.8	1051.4	.240	40'	4370.1	1476.4	.332	40'	5219.7	2021.1	.332
50'	3638.5	1057.7	T	50'	4383.3	1484.4	T	50'	5234.9	2031.4	T
65°	3650.2	1063.9	20° C.	75°	4396.5	1492.4	20° C.	85°	5250.3	2041.7	20° C.
10'	3661.9	1070.2	T	10'	4409.8	1500.5	T	10'	5265.6	2052.1	T
20'	3673.7	1076.6	.76	20'	4423.1	1508.6	.91	20'	5281.0	2062.5	.91
30'	3685.4	1082.9	E	30'	4436.4	1516.7	E	30'	5296.4	2073.0	E
40'	3697.2	1089.3	.240	40'	4449.7	1524.9	.332	40'	5311.9	2083.5	.332
50'	3709.0	1095.7	T	50'	4463.1	1533.1	T	50'	5327.4	2094.1	T
66°	3720.9	1102.2	25° C.	76°	4476.5	1541.4	25° C.	86°	5343.0	2104.7	25° C.
10'	3732.7	1108.6	T	10'	4489.9	1549.7	T	10'	5358.6	2115.3	T
20'	3744.6	1115.1	.76	20'	4503.4	1558.0	.91	20'	5374.2	2126.0	.91
30'	3756.5	1121.7	E	30'	4516.9	1566.3	E	30'	5389.9	2136.7	E
40'	3768.5	1128.2	.240	40'	4530.4	1574.7	.332	40'	5405.6	2147.5	.332
50'	3780.4	1134.8	T	50'	4544.0	1583.1	T	50'	5421.4	2158.4	T
67°	3792.4	1141.4	30° C.	77°	4557.6	1591.6	30° C.	87°	5437.2	2169.2	30° C.
10'	3804.4	1148.0	T	10'	4571.2	1600.1	T	10'	5453.1	2180.2	T
20'	3816.4	1154.7	.76	20'	4584.8	1608.6	.91	20'	5469.0	2191.1	.91
30'	3828.4	1161.3	E	30'	4598.5	1617.1	E	30'	5484.9	2202.2	E
40'	3840.4	1168.1	.240	40'	4612.2	1625.7	.332	40'	5500.9	2213.2	.332
50'	3852.6	1174.8	T	50'	4626.0	1634.4	T	50'	5517.0	2224.3	T
68°	3864.7	1181.6	35° C.	78°	4639.8	1643.0	35° C.	88°	5533.1	2235.5	35° C.
10'	3876.6	1188.4	T	10'	4653.6	1651.7	T	10'	5549.2	2246.7	T
20'	3889.0	1195.2	.76	20'	4667.4	1660.5	.91	20'	5565.4	2258.0	.91
30'	3901.2	1202.0	E	30'	4681.3	1669.2	E	30'	5581.6	2269.3	E
40'	3913.4	1208.9	.240	40'	4695.2	1678.1	.332	40'	5597.8	2280.6	.332
50'	3925.6	1215.8	T	50'	4709.2	1686.9	T	50'	5614.2	2292.0	T
69°	3937.9	1222.7	40° C.	79°	4723.2	1695.8	40° C.	89°	5630.5	2303.5	40° C.
10'	3950.2	1229.7	T	10'	4737.2	1704.7	T	10'	5646.9	2315.0	T
20'	3962.5	1236.7	.76	20'	4751.2	1713.7	.91	20'	5663.4	2326.5	.91
30'	3974.8	1243.7	E	30'	4765.3	1722.7	E	30'	5679.9	2338.2	E
40'	3987.2	1250.8	.240	40'	4779.4	1731.7	.332	40'	5696.4	2349.8	.332
50'	3999.5	1257.9	T	50'	4793.6	1740.8	T	50'	5713.0	2361.5	T
70°	4011.9	1265.0	45° C.	80°	4807.7	1749.9	45° C.	90°	5729.7	2373.3	45° C.
10'	4024.4	1272.1	T	10'	4822.0	1759.0	T	10'	5746.3	2385.1	T
20'	4036.8	1279.3	.76	20'	4836.2	1768.2	.91	20'	5763.1	2397.0	.91
30'	4049.3	1286.5	E	30'	4850.5	1777.4	E	30'	5779.9	2408.9	E
40'	4061.8	1293.6	.240	40'	4864.8	1786.7	.332	40'	5796.7	2420.9	.332
50'	4074.4	1300.9	T	50'	4879.2	1796.0	T	50'	5813.6	2432.9	T

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+
10'	5847.5	2457.1	5° C.	10'	6971.3	3294.1	5° C.	10'	8362.7	4407.6	5° C.
20'	5864.6	2469.3	T	20'	6992.0	3310.1	T	20'	8388.9	4429.2	T
30'	5881.7	2481.5	.43	30'	7012.7	3326.1	.51	30'	8415.1	4450.9	.62
40'	5898.8	2493.8	E	40'	7033.6	3342.3	E	40'	8441.5	4472.7	E
50'	5916.0	2506.1	.200	50'	7054.5	3358.5	.268	50'	8468.0	4494.6	.360
92°	5933.2	2518.5	10° C.	102°	7075.5	3374.9	10° C.	112°	8494.6	4516.6	10° C.
10'	5950.5	2531.0	T	10'	7096.6	3391.2	T	10'	8521.3	4538.8	T
20'	5967.9	2543.5	.86	20'	7117.8	3407.7	.103	20'	8548.1	4561.1	.125
30'	5985.3	2556.0	E	30'	7139.0	3424.3	E	30'	8575.0	4583.4	E
40'	6002.7	2568.6	.604	40'	7160.3	3440.9	.536	40'	8602.1	4606.0	.721
50'	6020.2	2581.3	T	50'	7181.7	3457.6	T	50'	8629.3	4628.6	T
93°	6037.8	2594.0	15° C.	103°	7203.2	3474.4	15° C.	113°	8656.6	4651.3	15° C.
10'	6055.4	2606.8	T	10'	7224.7	3491.3	T	10'	8684.0	4674.2	T
20'	6073.1	2619.7	.86	20'	7246.3	3508.2	.103	20'	8711.5	4697.2	.125
30'	6090.8	2632.6	E	30'	7268.0	3525.2	E	30'	8739.2	4720.3	E
40'	6108.6	2645.5	.604	40'	7289.8	3542.4	.536	40'	8767.0	4743.6	.721
50'	6126.4	2658.5	T	50'	7311.7	3559.6	T	50'	8794.9	4766.9	T
94°	6144.3	2671.6	20° C.	104°	7333.6	3576.8	20° C.	114°	8822.9	4790.4	20° C.
10'	6162.2	2684.7	T	10'	7355.6	3594.2	T	10'	8851.0	4814.1	T
20'	6180.2	2697.9	.86	20'	7377.8	3611.7	.103	20'	8879.3	4837.8	.125
30'	6198.3	2711.2	E	30'	7399.9	3629.2	E	30'	8907.7	4861.7	E
40'	6216.4	2724.5	.604	40'	7422.2	3646.8	.536	40'	8936.3	4885.7	.721
50'	6234.6	2737.9	T	50'	7444.6	3664.5	T	50'	8965.0	4909.9	T
95°	6252.8	2751.3	25° C.	105°	7467.0	3682.3	25° C.	115°	8993.8	4934.1	25° C.
10'	6271.1	2764.8	T	10'	7489.6	3700.2	T	10'	9022.7	4958.6	T
20'	6289.4	2778.3	.86	20'	7512.2	3718.2	.103	20'	9051.7	4983.1	.125
30'	6307.9	2792.0	E	30'	7534.9	3736.2	E	30'	9080.9	5007.8	E
40'	6326.3	2805.6	.604	40'	7557.7	3754.4	.536	40'	9110.3	5032.6	.721
50'	6344.8	2819.4	T	50'	7580.5	3772.6	T	50'	9139.8	5057.6	T
96°	6363.4	2833.2	30° C.	106°	7603.5	3791.0	30° C.	116°	9169.4	5082.7	30° C.
10'	6382.1	2847.0	T	10'	7626.6	3809.4	T	10'	9199.1	5107.9	T
20'	6400.8	2861.0	.86	20'	7649.7	3827.9	.103	20'	9229.0	5133.3	.125
30'	6419.5	2875.0	E	30'	7672.9	3846.5	E	30'	9259.0	5158.8	E
40'	6438.4	2889.0	.604	40'	7696.3	3865.2	.536	40'	9289.2	5184.5	.721
50'	6457.3	2903.1	T	50'	7719.7	3884.0	T	50'	9319.5	5210.3	T
97°	6476.2	2917.3	35° C.	107°	7743.2	3902.9	35° C.	117°	9349.9	5236.2	35° C.
10'	6495.2	2931.6	T	10'	7766.8	3921.9	T	10'	9380.5	5262.3	T
20'	6514.3	2945.9	.86	20'	7790.5	3940.9	.103	20'	9411.3	5288.6	.125
30'	6533.4	2960.3	E	30'	7814.3	3960.1	E	30'	9442.2	5315.0	E
40'	6552.6	2974.7	.604	40'	7838.1	3979.4	.536	40'	9473.2	5341.5	.721
50'	6571.9	2989.2	T	50'	7862.1	3998.7	T	50'	9504.4	5	

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

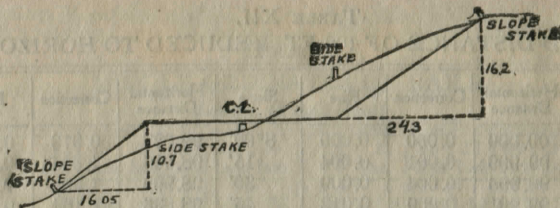
TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

70
9.4
5
1
9
526
3/24
2000

4445 1/2 nail in 16" block
 use a temp



225
 370

360
 35230

159
 30

365 on Col 5 with line to Swamp 76
 107
 99.4

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER
 COURT HOUSE
 CHARDON, O.
 PHONE 250-X

36030
 29630

2330
 34
 6220

242
 55

2830
 2.1

13
 16
 98
 13
 208

125
 16
 780
 125
 2000

180
 2830
 130



3-5-5 to road
 190 on " - Potline to Bridge
 650 " " " PnceWm
 590 BM to Beaver ck
 675 " " " Slas"
 465 across 10th Busz Prop
 413 Billeke car to int tangwa
 Harris
 Hawkick S line N. 84° E.
 " " " N 83° E

526
 324
 Stamp

